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AD 911384



AD

Research and Development Technical Report
ECOM-0129-F

WATER ACTIVATED ZINC-SILVER OXIDE

PRIMARY BATTERY

FINAL REPORT

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RECORDED
JUL 2 1973
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By
C. C. BROWN

JUNE, 1973

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ECOM

UNITED STATES ARMY ELECTRONICS COMMAND · FORT MONMOUTH, N.J.

CONTRACT DAAB07-71-C-0129

EAGLE-PICHER INDUSTRIES, INC.
Joplin, Missouri

Distribution limited to US Government agencies only; covers the test and evaluation, 6 June 73. Other requests for this document must be referred to Commander, US Army Electronics Command, ATTN: AMSEL-TL-PD, Fort Monmouth, New Jersey 07703

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JUNE 1973

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WATER ACTIVATED ZINC-SILVER OXIDE
PRIMARY BATTERY

FINAL REPORT

16 February 1971 to 15 March 1973

CONTRACT NO. DAAB07-71-C-0129
DA PROJECT NO. 1T0627 05A 0530277

Prepared by
C. C. Brown

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Couples Department
Electronics Division
Eagle-Picher Industries, Inc.
Joplin, Missouri

For

U. S. ARMY ELECTRONICS COMMAND, FORT MONMOUTH, N. J.

ABSTRACT

This report describes the design, development, manufacture and evaluation testing of a Zinc-Silver Oxide reserve battery in accordance with "Technical Guidelines for Water Activated Zinc-Silver Oxide Battery". This includes a description of the design effort, the design, the test program, the test equipment and the test results. The evaluation testing showed compliance with the requirements of the technical guidelines.

FOREWORD

This work was performed for Power Sources Division, Electronics Components Laboratory, U.S. Army Electronics Command, Fort Monmouth, New Jersey, under Contract DAAB07-71-C-0129. This report is prepared in accordance with DD1423, Exhibit A under the above contract and is intended to describe the complete program.

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1.0 GENERAL

The work performed under this contract consisted of the design, development and fabrication of sixty (60) batteries as described in the following paragraphs and selection of thirty (30) of these units for test in accordance with 2-f of "Technical Guidelines for Water Activated Zinc-Silver Oxide Battery" and Table I herein.

2.0 DESIGN FEATURES

2.1 Cell Design

The cell design effort was begun with the design approach described in Eagle-Picher proposal EPP-1170-474/DMH which was in turn based on an Eagle-Picher internally developed battery with performance characteristics similar to those required by this contract. The proposed design called for one (1) negative and two (2) positive plates in each cell. The area of each of these plates was 5.25 square inches and the total weight of positive material was 28.8 grams and of negative material was 23.6 grams. Cells were fabricated with this plate design and with two (2) layers of membrane separation on the positive plate and one (1) layer of absorbent separation on the negative plate. These cells, when tested, failed to yield the required capacity before the cutoff voltage was reached. When approximately half of the expected capacity was expended the voltage dropped noticeably to a lower level which was maintained for a short time then gradually decreased to the point of cutoff. These voltage characteristics can be seen in the curve of Figure 1.

These cells were disassembled and it was determined that the active material was not being completely utilized because the potassium hydroxide electrolyte was not being dispersed enough to completely activate the positive plates. In order to correct this cells were fabricated with a layer of absorbent separation between the positive plate and the membrane separation and other cells with no separation on the positive plate and with two (2) layers of both membrane and absorbent separation on the negative plate. Neither of these designs produced any significant improvement in the performance.

The next step was to fabricate cells with the same positive plate area and active material as the first design but only half the length of the first design. This produced a cell with four (4) positive and three (3) negative plates. Since the same weight plates were used as the original design, excess negative material was in the cell because three (3) plates were required to balance the four (4) positive plates. These cells produced the expected capacity, 8.9 ampere hours, at a voltage .05 to .08 VDC above that of the first design.

Cells were then fabricated using the shorter plate design but with lighter negative plates to provide the proper active material ratio, positive-to-negative. In order to fit the specified battery outline, these plates were shorter than the first half-length cells. These changes resulted in a design with six (6) positive and five (5) negative plates each of 1.69 square inches, producing a total negative area of 8.55 square inches and positive area of 10.12 square inches. The negative material weight is 21.0 grams for the five (5) plates

and the positive material weight is 30.35 grams for six (6) plates. These cells provided good voltage and capacity in excess of that required by the specification.

2.2 Case Design

The major controlling factor in the case design was the cell configuration which would meet the specified electrical requirements. Because a short multiple plate cell was required to achieve the required electrical performance, the orientation of the cells would have to be across the short dimension of the specified envelope. With this cell configuration, the method of activation must then be determined.

The cells will activate quicker from the end because the separation is open at the end allowing the water to flow directly in between the layers of separation and the plates. The short cell configuration described above fits into the specified envelope leaving room for the activation channel along one side and the connector on the end as shown in Figure 2. In order to prevent electrolyte leakage and allow escape of the gases generated during stand and discharge, porous teflon vent filters, also shown in Figure 2, were provided at both ends of the cells. This allows the gas to escape freely with the battery in any position since both vents could not be covered by electrolyte at the same time.

The first method of sealing tried was to provide a neoprene gasket, on all of the cells, which would be compressed by the cover which contained the vent filters. Leakage occurred around the neoprene gasket which was attributed to uneven compression of the gasket.

The next sealing method tried consisted of providing a common manifold which activated all cells, reference Figure 2. An expansion stopper is provided in the end of this manifold through which the water can be added. After completion of the activation, the stopper is then installed in the activation port to prevent electrolyte leakage. The gas generated after activation is vented through the porous teflon filters. This method worked well in sealing the unit. Although there was some free electrolyte left in the manifold during discharge, there was no leakage.

This case was fabricated from plastic (MIL-P-21105). The vibration and shock tests were performed on this case with no detrimental effects. The first batteries fabricated had the plate leads and intercell connectors on the end opposite the activation manifold. This resulted in shorting between the plates and the plate leads. The shorting was caused by insufficient clearance between the plates and the end of the cell case. On the other batteries fabricated, the intercell connections and plate leads were placed on the end next to the activation manifold where there was more head room. This type of fabrication prevented shorting of the plate lead wires.

3.0 BATTERY FABRICATION

The batteries were assembled in plastic cases (Figure 2) which were fabricated here in our plant. After formation of the positive plate strips, the plates were cut to size and wrapped with separation. The negative plates are cut to sized and wrapped with separator then placed alternately with the positive plates to make a cell. The cells are immediately inserted

into the case as they are assembled. After all the cells are placed into the case, the cover is installed and sealed in place. The cells are then interconnected and lead wires routed to the power output connector. The cell interconnections are then covered with potting. The top and bottom vent strips are then installed and sealed. The units are then painted and the labels and activation plug installed.

4.0 TEST PERFORMANCE

The test units were loaded as follows:

Section	Condition A		Condition B	
	2 min. Load 1 (ohms)	18 min. Load 2 (ohms)	Continuous Load (ohms) N/A	End Voltage
A ₁	6.76 ± 1%	O.C.		2.12
A ₂	14.2 ± 1%	291 ± 1%	28.75 ± 1%	10.0

The actual test setup was as shown in Figures 3 and 4.

The batteries were activated with water stabilized for 8 hours minimum at the same temperature as the battery except when the battery was below 40°F. Then the water was stabilized for 8 hours minimum at 40°F. The Immediate Discharge Tests were started five (5) minutes after the start of activation.

When specified, shock and vibration loads as follows were applied to the test unit:

Vibration: Sine, 0.06 in DA

Sweep, 1 cpm from 10 to 55 to 10 cps

Duration, 95 ± 5 min/axis, 3 axis

Shock: Average acceleration during first 3ms is 75 g's

Peak acceleration, 125 to 175 g's

One shock in each of 3 directions

Three shocks total

The batteries were activated in accordance with the instructions attached to each battery which is as follows. The battery was removed from its protective packaging and held in the vertical position with

TABLE I
TEST PLAN

<u>TEST DESCRIPTION</u>	<u>LOAD CONDITION</u>	<u>SPECIMEN NUMBERS</u>
Immediate Discharge at 75°F	A	1 - 4
Immediate Discharge at 125°F		5 - 6
Immediate Discharge at 0°F		7 - 8
Immediate Discharge at -20°F		9 - 10
Discharge at 75°F following 7 days activated storage at 75°F		11 - 12
Discharge at 75°F following 100 hours activated storage at 125°F		13 - 14
Immediate Discharge at 75°F following exposure to mechanical vibration and shock		15 - 16
Immediate Discharge at 75°F while being exposed to mechanical shock		17 - 18
Immediate Discharge at 75°F while being exposed to vibration	A	19 - 20
Immediate Discharge at 75°F	B	21 - 22
Immediate Discharge at 125°F		23 - 24
Immediate Discharge at 0°F		25 - 26
Immediate Discharge at -20°F		27 - 28
Discharge at 75°F following 7 days activated storage at 75°F	B	29 - 30

the activation opening at the top (Ref. Figure 2). The unit was filled with water and held in that position for two (2) minutes, then the unit was filled again and rotated 180° so that the activation opening was at the bottom and held in that position two (2) minutes. The plug was then removed and the excess water poured out and the plug was again installed. All activations were completed in the five (5) minutes allowed.

5.0 TEST SUMMARY

Table II gives a summary of test results for the thirty (30) units tested. The low temperatures produced marginal results in the A₁ Section, when discharged at Condition A. This was especially noted at -20°F. This is probably due to the location of the cells being on the end of the battery and their load being open circuit 90% of the time, results in their temperature being lower than average temperature of the cells in the A₂ Section. The A₂ Section was marginal at 0°F and very poor at -20°F when discharged at Load Condition B. The only reason that could be determined for poor operation at Condition B loads was the difference in the rate.

Low capacity in the A₁ Section of Specimens 11, 14, 15 and 16 was experienced during original testing caused by a cell-to-cell short through a poor seal around the bottom vent opening as shown in Figure 5. This opening in the seal allowed zinc dendrites to form between the cells producing a high resistance short. This could be prevented on future batteries fabricated by placing individual vent patches over the bottom vents as shown in Figure 6.

This would not change the seal method but would permit inspection of each seal to verify that no voids are in the seal. This method was used on five (5) units which were tested to the original environments where the shorting occurred. There was no shorting in any of these units. The thirty (30) units delivered have the revised seals in accordance with Figure 6.

TABLE II
SUMMARY OF TEST RESULTS

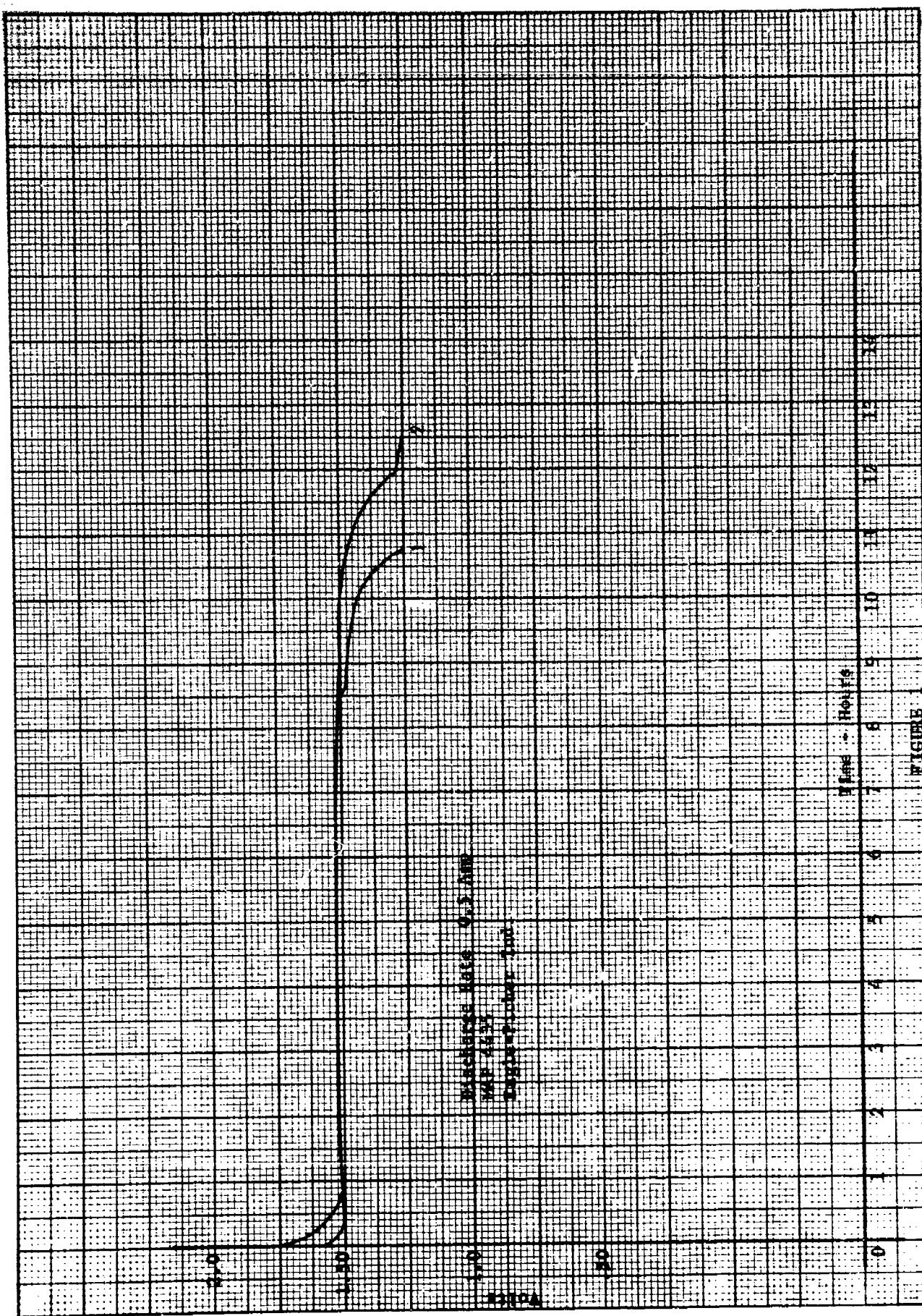
SPEC. NO.	SERIAL NO.	TEST DESCRIPTION	A ₁ SECTION (HOURS)		A ₂ SECTION (HOURS)		Required Results	Results	Required Results	TEST DATE COND.	LOAD A
			A ₁	A ₂	A ₁	A ₂					
1	14	Immediate Discharge at 75°F	60	108	60	68	6/5/72				
2	11	Immediate Discharge at 75°F	60	123	60	78	6/5/72				
3	60	Immediate Discharge at 75°F	60	97	60	81	6/5/72				
4	1	Immediate Discharge at 75°F	60	84	60	71	6/5/72				
5	4	Immediate Discharge at 125°F	60	89	60	81	6/5/72				
6	13	Immediate Discharge at 125°F	60	87	60	74	6/5/72				
7	19	Immediate Discharge at 0°F	50	84	50	72	6/27/72				
8	45	Immediate Discharge at 0°F	50	80	50	72	6/27/72				
9	37	Immediate Discharge at -20°F	30*	69	30*	23	6/13/72				
10	54	Immediate Discharge at -20°F	30*	52	30*	12	6/13/72				
11	78	Discharge at 75°F following 7 day activated stand at 75°F	50	68	50	60	6/13/72				
12	42	Discharge at 75°F following 7 day activated stand at 75°F	50	86	50	82	6/13/72				
13	22	Discharge at 75°F following 100 hour activated stand at 125°F	50	62	50	75	6/13/72				
14	47	Discharge at 75°F following 100 hour activated stand at 125°F	50	76	50	76	6/13/72				
15	74	Immediate Discharge at 75°F following exposure to mechanical vibration and shock	60	90	60	79	6/19/72				
16	24	Immediate Discharge at 75°F following exposure to mechanical vibration and shock exposed to mechanical shock	60	64	60	78	6/19/72				
17	5	Immediate Discharge at 75°F while being exposed to mechanical shock	60	87	60	80	6/19/72				
18	7	Immediate Discharge at 75°F while being exposed to mechanical shock	60	101	60	77	6/19/72				
19	8	Immediate Discharge at 75°F while being exposed to vibration	60	103	60	79	6/19/72				
20	34	Immediate Discharge at 75°F while being exposed to vibration	60	102	60	82	6/19/72				
21	9	Immediate Discharge at 75°F	N/A	N/A	18	26:45	6/5/72				
22	18	Immediate Discharge at 75°F			18	18	6/5/72				
23	20	Immediate Discharge at 125°F			18	25	6/7/72				
24	59	Immediate Discharge at 125°F			18	26	6/7/72				
25	46	Immediate Discharge at 0°F			15	15:15	6/14/72				
26	31	Immediate Discharge at 0°F			15	16:50	6/14/72				

Continued on next page

TABLE II (Continued)

Spec. No.	Serial No.	Test Description	A ₁ SECTION		A ₂ SECTION		Load Cond.
			(Hours)	Required Results	(Hours)	Required Results	
27	21	Immediate Discharge at -20°F	N/A	N/A	10*	5	6/13/72
28	53	Immediate Discharge at -20°F			10*	1	6/13/72
29	35	Discharge at 75°F following 7 day activated stand at 75°F			15	23	6/7/72
30	36	Discharge at 75°F following 7 day activated stand at 75°F	N/A	N/A	15	24	6/7/72

* -20°F Test is a Design Goal.



MAP 4435 ACTIVATION SYSTEM
AND ASSEMBLY LAYOUT

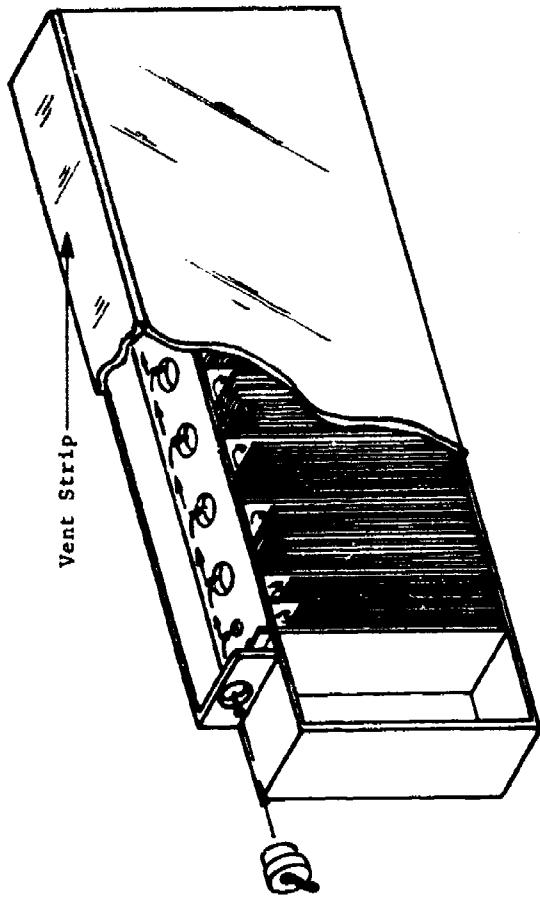
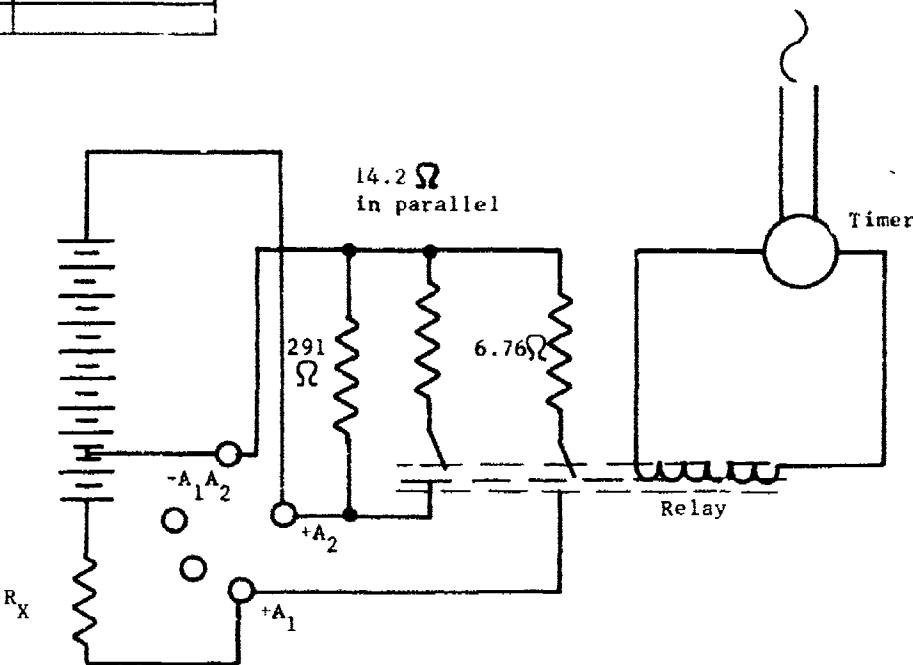


FIGURE 2

APPLICATION		REVISIONS			
NEXT ASSY	USED ON	LTR	DESCRIPTION	DATE	APPROVED



UNLESS OTHERWISE SPECIFIED
DIMENSIONS ARE IN INCHES
TOLERANCES: FRACTIONS $\pm \frac{1}{16}$
ANGLES $\pm 5^\circ$
3 PLACE DECIMALS $\pm .010$
2 PLACE DECIMALS $\pm .03$

CONTRACT NO.



EAGLE PITCHER INDUSTRIES, INC.
COUPLES DEPARTMENT
JOPLIN, MISSOURI



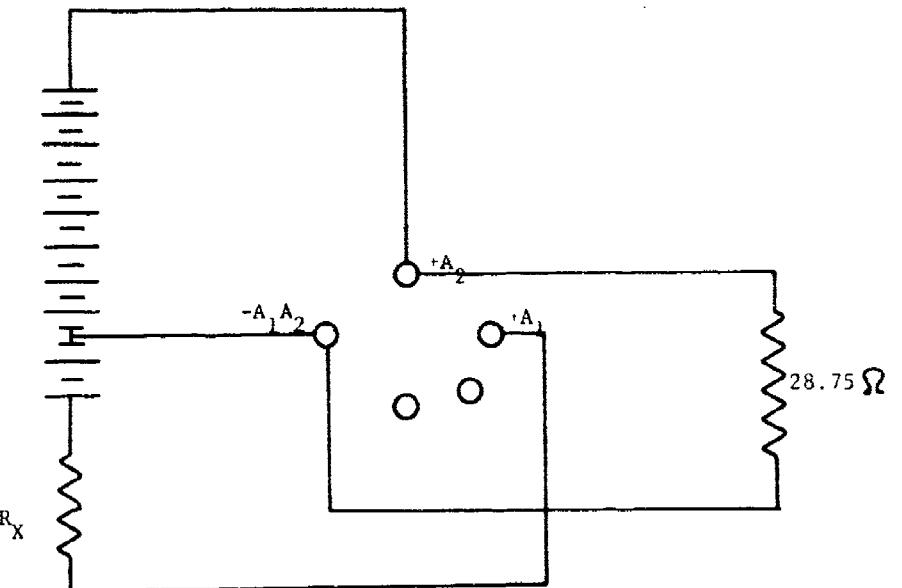
DATE _____

DISCHARGE SCHEMATIC LOAD CONDITION A

PREPARED	
CHECKED	
ENGINEER	

SIZE	CODE IDENT NO.	DRAWING NO.
A	81855	FIGURE 3
SCALE		SHEET

APPLICATION		REVISIONS			
NEXT ASSY	USED ON	LTR	DESCRIPTION	DATE	APPROVED



UNLESS OTHERWISE SPECIFIED
DIMENSIONS ARE IN INCHES
TOLERANCES: FRACTIONS \pm
ANGLES \pm
3 PLACE DECIMALS $\pm .010$
2 PLACE DECIMALS $\pm .03$

CONTRACT NO.

DATE _____



EAGLE PITCHER INDUSTRIES, INC.
COUPLES DEPARTMENT
JOPLIN, MISSOURI



DISCHARGE SCHEMATIC LOAD CONDITION 6

PREPARED _____
CHECKED _____
ENGINEER _____

SIZE CODE IDENT NO. DRAWING NO.

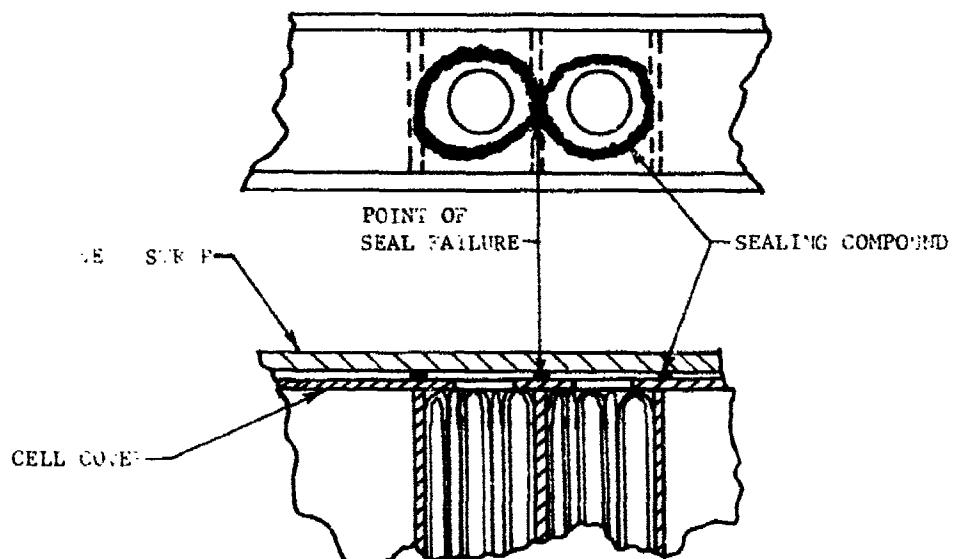
A 81855

FIGURE 4 SHEET

SCALE

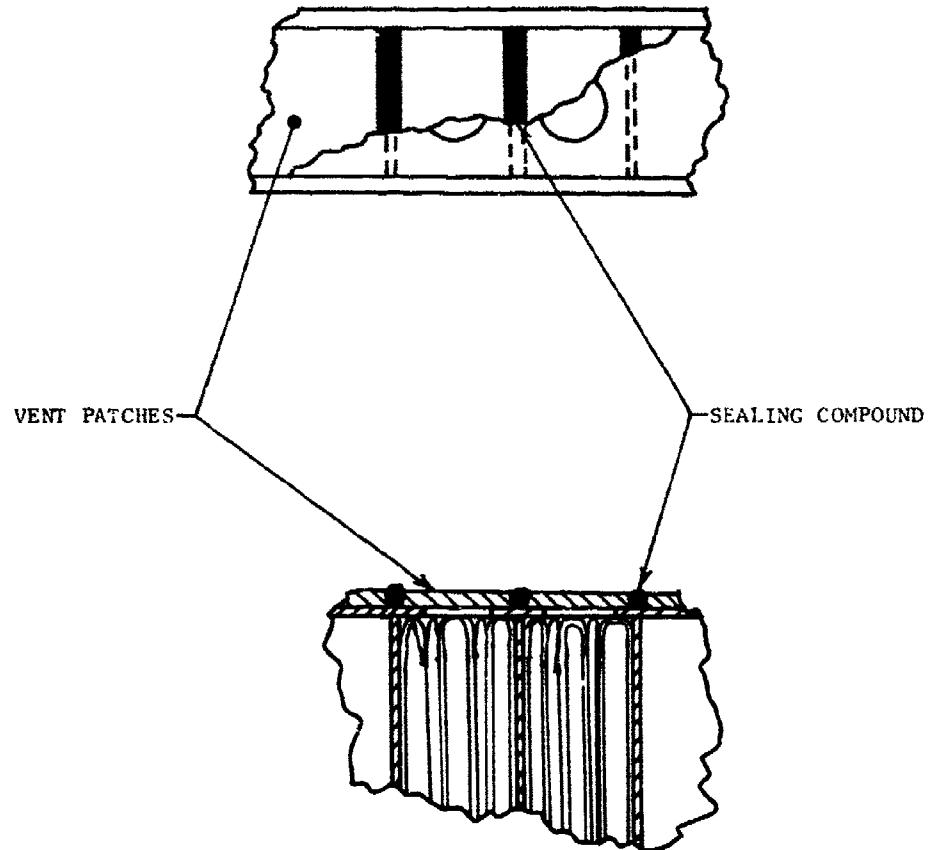
APPLICATION		REVISIONS		
NEXT ASSY	USED ON	LTR	DESCRIPTION	DATE APPROVED

VENT STRIP NOT
SHOWN ON TOP VIEW



UNLESS OTHERWISE SPECIFIED DIMENSIONS ARE IN INCHES TOLERANCES: FRACTIONS $\pm \frac{1}{16}$ ANGLES $\pm 5^\circ$ 3 PLACE DECIMALS $\pm .010$ 2 PLACE DECIMALS $\pm .03$		CONTRACT NO. _____		EAGLE PITCHER INDUSTRIES, INC. COUPLES DEPARTMENT JOPLIN, MISSOURI	
		DATE _____			
		PREPARED		EP	
		CHECKED		EP	
		ENGINEER			
		ORIGINAL VENT SEAL			
		SIZE	CODE IDENT NO.	DRAWING NO.	
		A	81855	FIGURE 5	
		SCALE	N/A	SHEET	

APPLICATION		REVISIONS			
NEXT ASSY	USED ON	LTR	DESCRIPTION	DATE	APPROVED



UNLESS OTHERWISE SPECIFIED DIMENSIONS ARE IN INCHES TOLERANCES: FRACTIONS \pm ANGLES \pm 3 PLACE DECIMALS $\pm .010$ 2 PLACE DECIMALS $\pm .03$	CONTRACT NO.	EAGLE PITCHER INDUSTRIES, INC. COUPLES DEPARTMENT JOPLIN, MISSOURI	
	DATE _____	EP	
	PREPARED _____		
	CHECKED _____		
	ENGINEER _____		
		REVISED VENT SEAL	
		SIZE A	CODE IDENT NO. 81855
		DRAWING NO. FIGURE 6	
		SCALE N/A	SHEET

APPENDIX I

TEST DATA

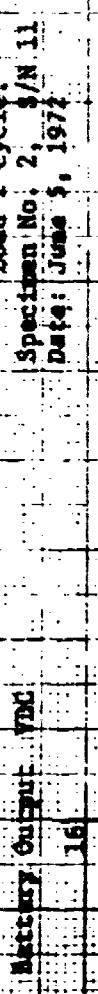
Battery - 2P P/N 44-4435
Discharge Voltage, Time
Intermediate Discharge at 15°
Rate = 100% capacity load - 1 sec

Discharge time - hours

A1 Section



A2 Section

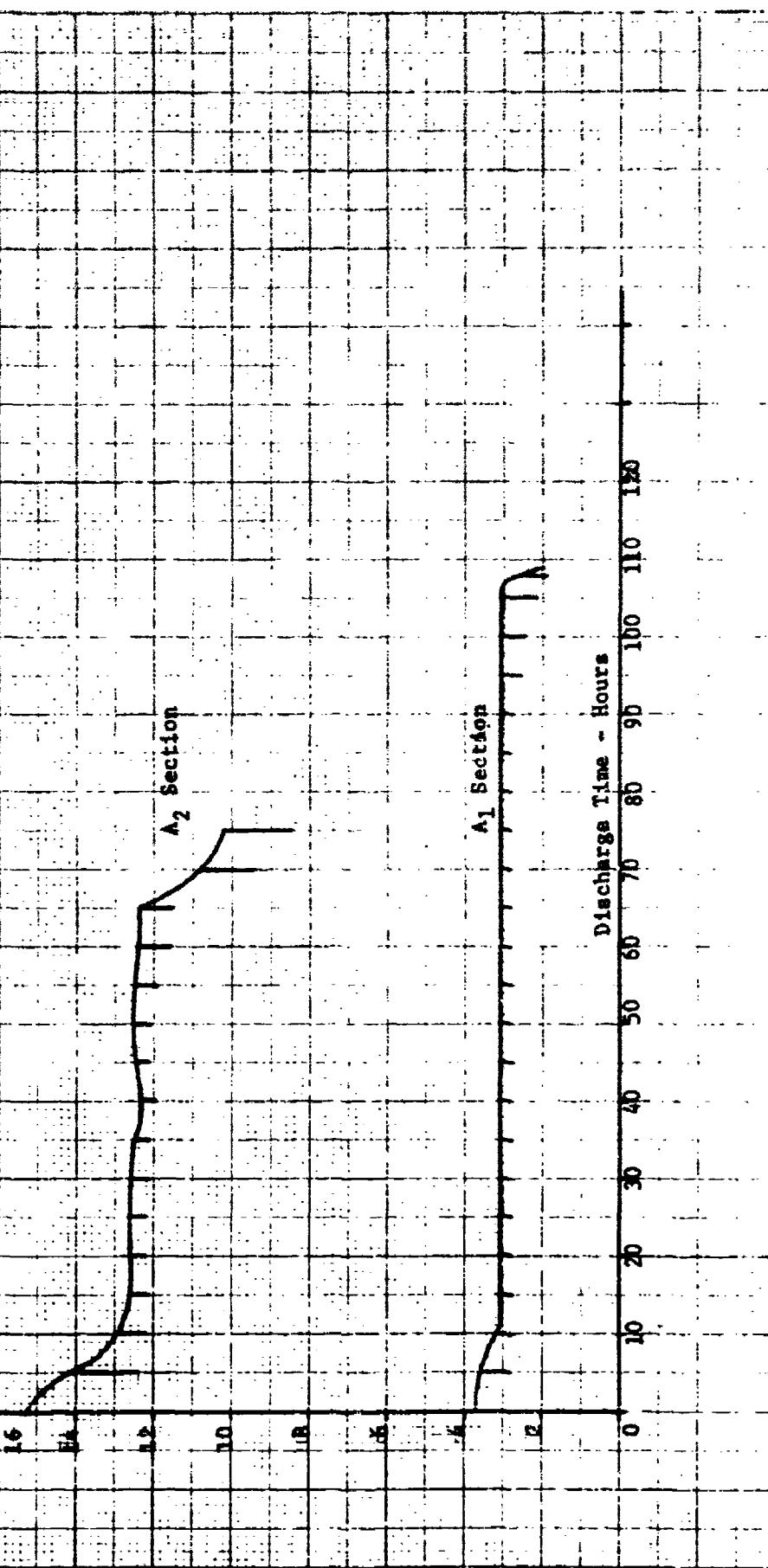


Specimen No. 2 Date: June 5, 1971
Specimen No. 1 Date: June 5, 1971
Tested at 100% capacity load - 1 sec
Loading was a 2 min. load in 10 min
shown at 5 hr. intervals.
Note - pre-circuit load - 1 sec

Battery EP P/N MAP 4435
Discharge Voltage vs. Time
Immediate Discharge at 75°F
Note: For clarity, load 1 surges
are shown at 1-hour intervals.
Actual loading was a 2 min. load 1,
13 min. load 2 cycles.

Specimen No.: 1, S/N 44-
Date: June 5, 1972

Battery Discharge



ESER EA - HOMECOMING '72
K-2

Battery E8 P/N NAP 4435
Discharge Voltage vs. Time
Immediate Discharge at 75°F
Note: For clarity load changes are
shown at 1 hr. intervals. Actual
loading was a 2 min. load 14.18 min.
Load 2 cycles:
Specimen No. 3, S/N 60
Date: June 5, 1972

BATTERY VOLTAGE - VDC

16

14

12

10

8

6

4

2

0

A1 section

100 110 120

0

10

20

30

40

50

60

70

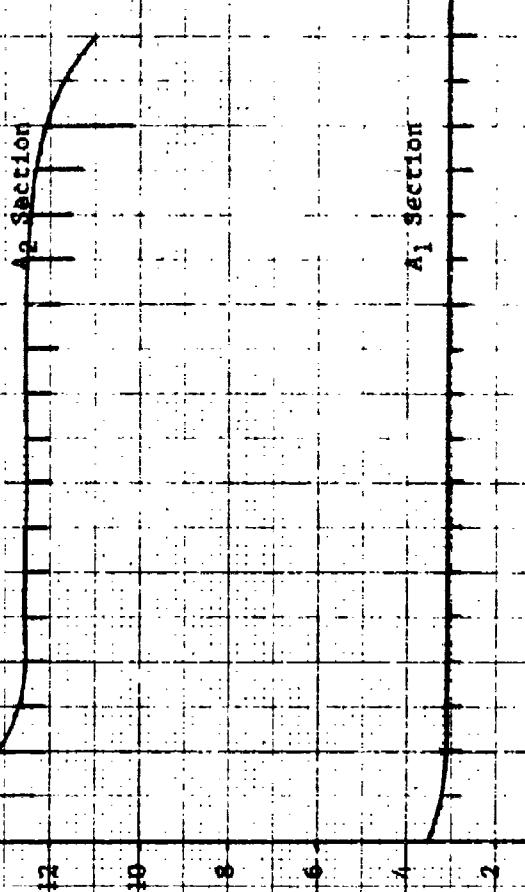
80

90

100

110

120



Battery EP-P/N MAP-4435

Discharge Voltage vs. Time

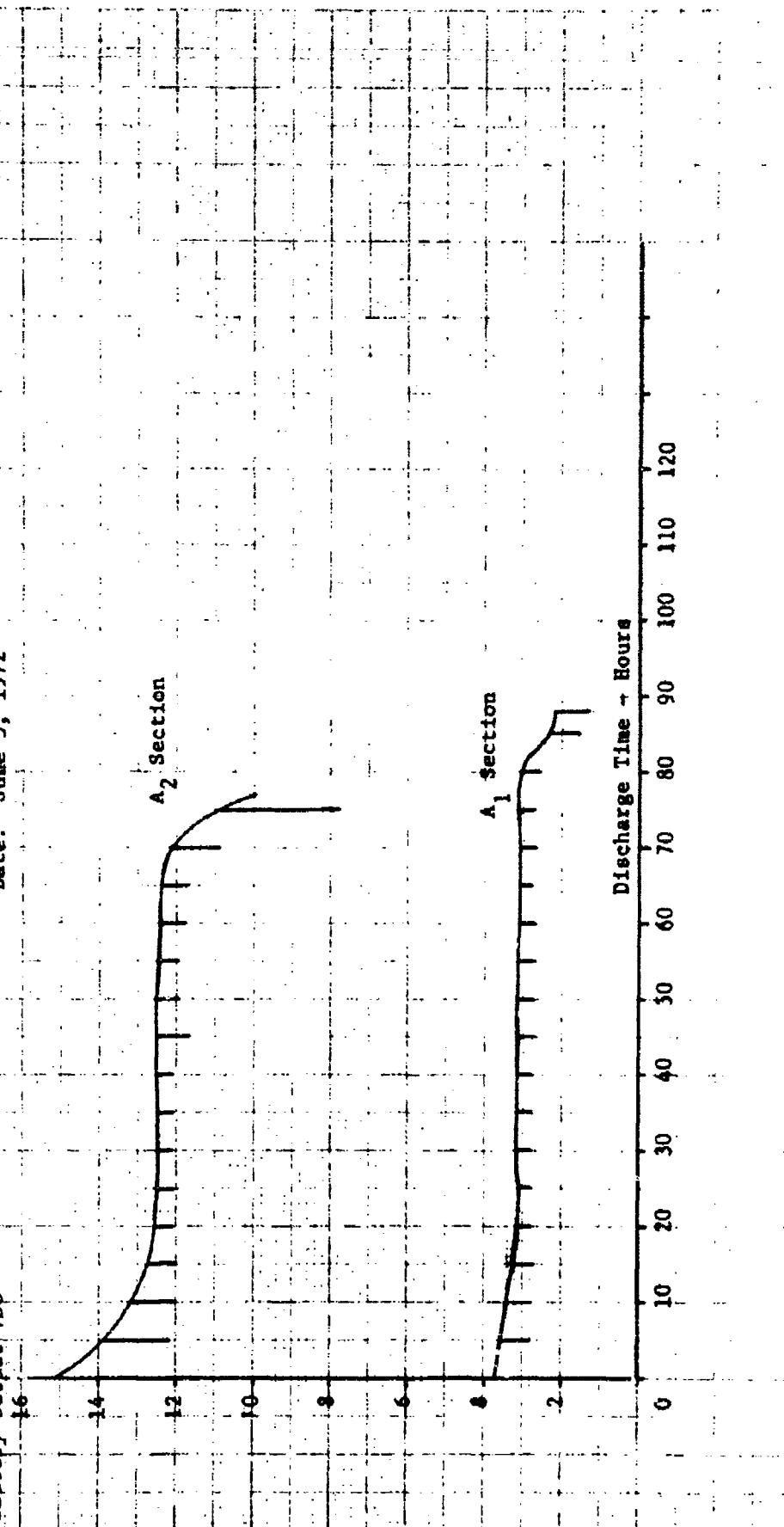
Immediate Discharge at 75° F.

Note: For clarity, Load 1 surges are shown at 5 hr. intervals. Actual loading was a 2 min Load 1, 18 min load 2.

Specimen No. 4, S/N 1

Date: June 5, 1972

Battery Output vDC



Battery E* P/N MAP 4435

Discharge Voltage vs. Time

Immediate Discharge at 125°F

Note: For clarity, Load 1 surges are shown at 5 hr. intervals. Actual loading was a 2 min. Load-1, 18 min.

Load 2, cycle.

Specimen No. 5, S/N 4

Date: June 5, 1972

Battery Output - VDC

16

14

12

10

8

6

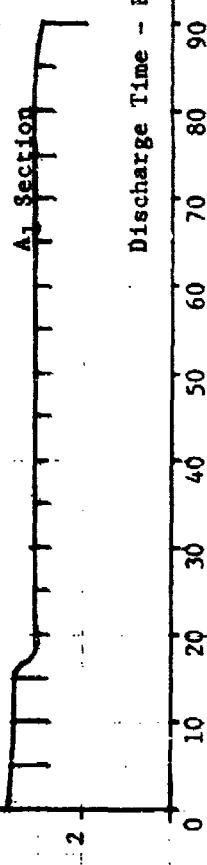
4

2

A₂ Section



A₁ Section



Discharge Time - Hours

0 10 20 30 40 50 60 70 80 90 100 110 120

Battery EP P/N MAP-4435

Discharge Voltage vs. Time

Immediate Discharge at 125°F

Note: For clarity, Load 1 surges are

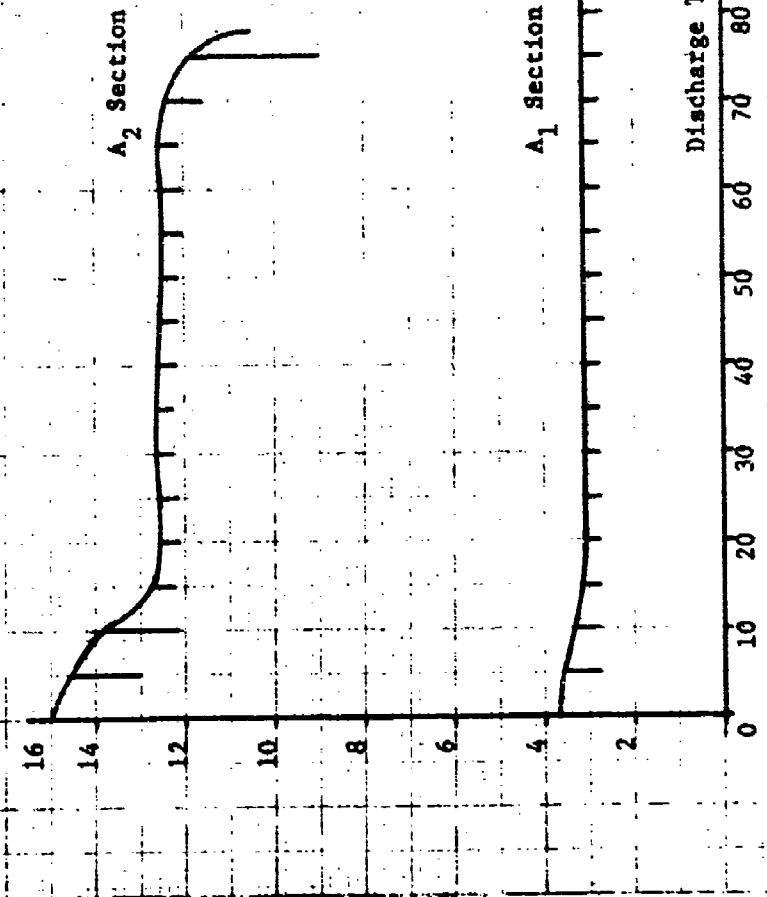
shown at 5 hr. intervals. Actual
loading was a 2 min. Load 1, 18 min.

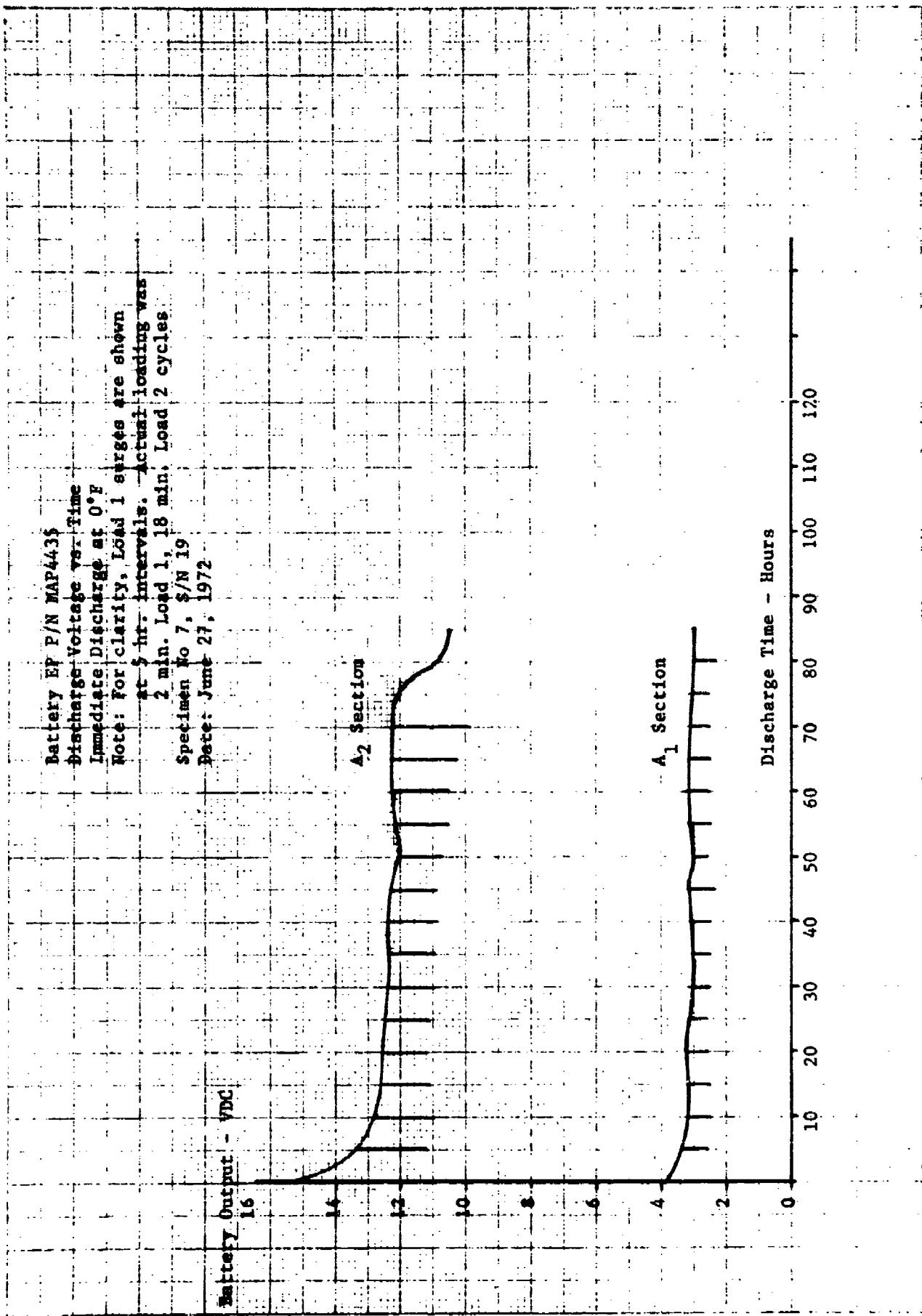
- Load 2, cycle.

Specimen No. 6, S/N 13

Date: June 5, 1972

Battery Output - VDC





Battery EP P/N MAP 4435

Discharge Voltage vs. Time

Immediate Discharge at 0° P

Note: For clarity, Load 1 surges are shown at 1 hr. interval. Actual load cycling was 2 min. Load 1 18 min.

Load 2 cycle

Specimen No. 8, S/N 43

Date: June 27, 1972

Battery Output-VDC

16

14

12

10

8

6

4

2

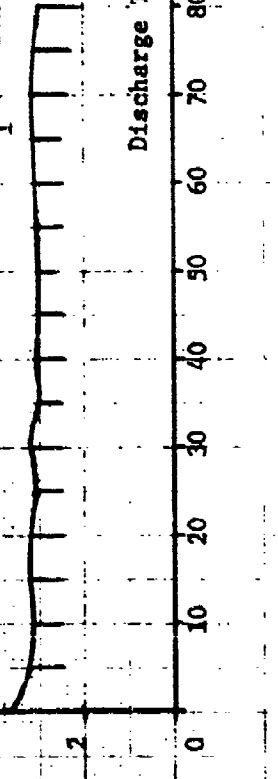
0

A₂ Section



26

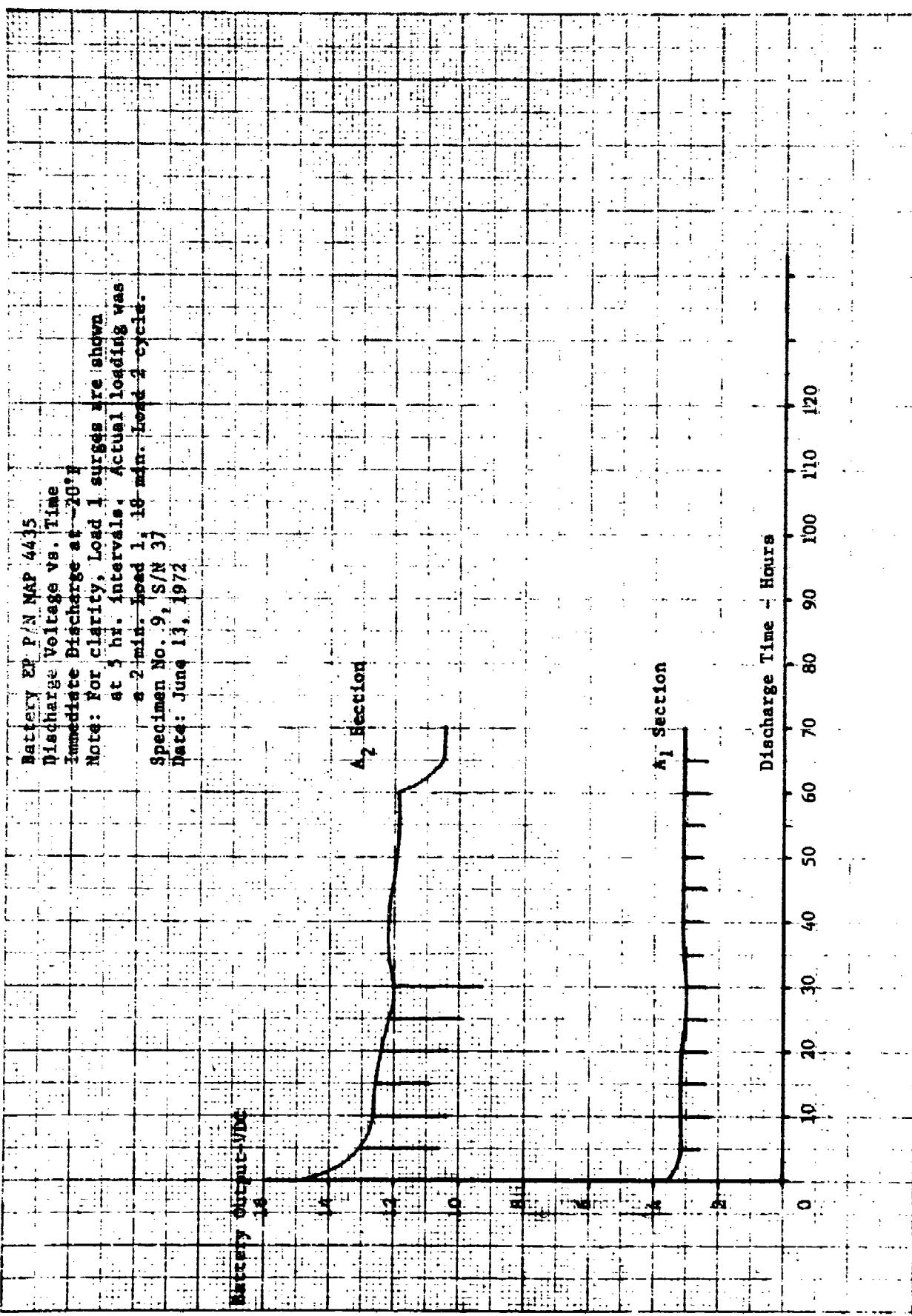
A₁ Section



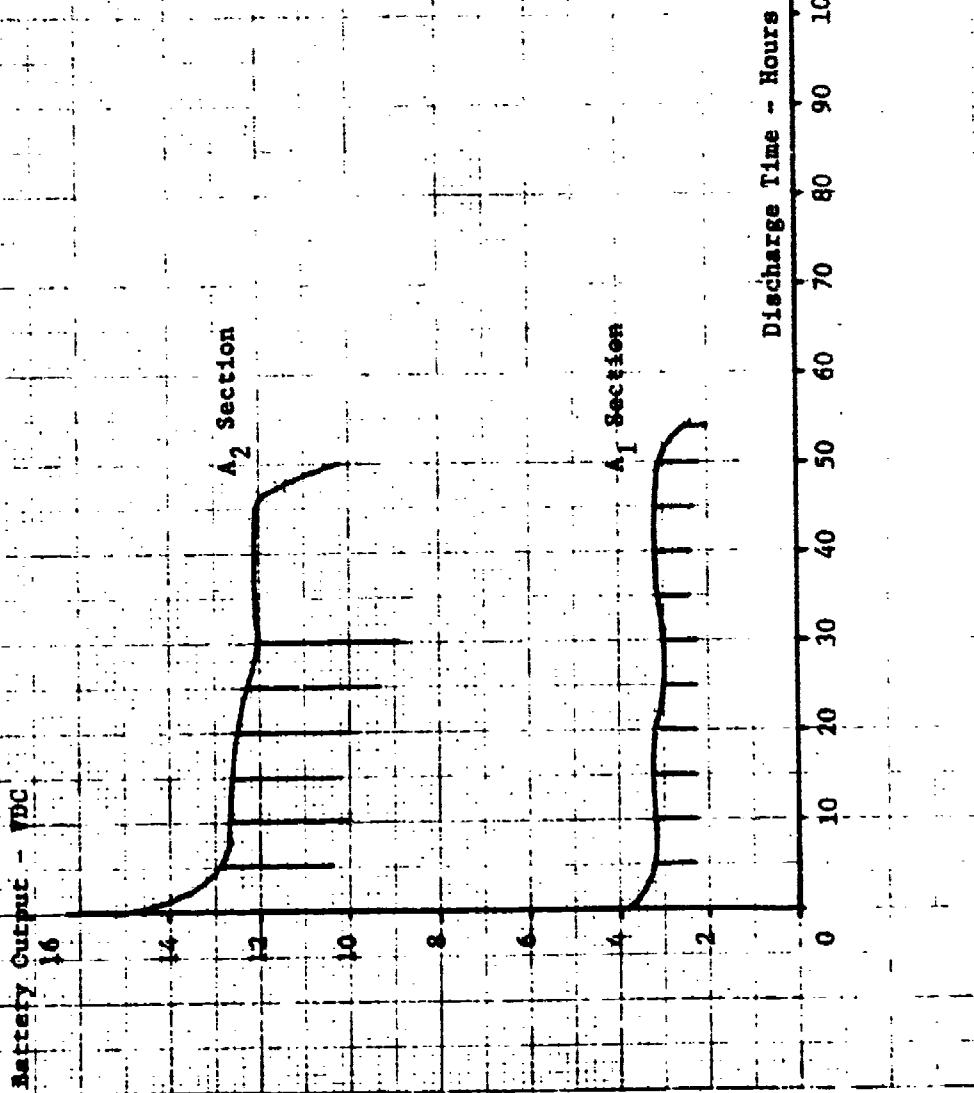
Discharge Time - Hours

120
110
100
90
80
70
60
50
40
30
20
10
0

ESER IN A SUBSTITUTION OF ORIGINATOR



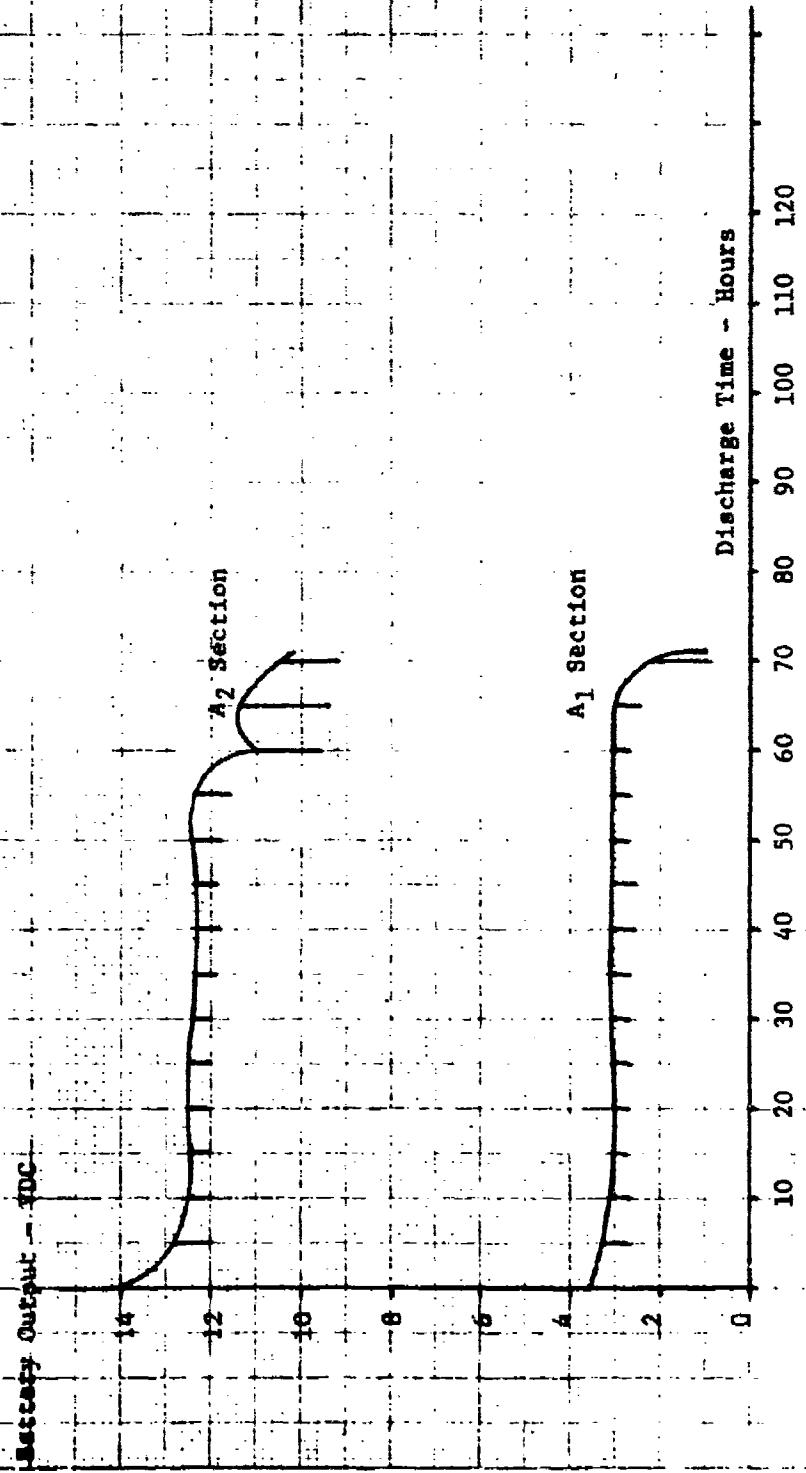
Battery EP P/N MAP 4435
Discharge Voltage vs. Time
Immediate Discharge at -20°F
Note: For clarity, Load 1 surges are shown
at 5 hrs. Actual loading was a 2-min.
Load 1: 16 min. Load 2 cycle
Specimen No. 10, S/N 54
Date June 13, 1972



Specimen No. 11 S/N 78

Battery EP P/N MAP 4435
Discharge Voltage vs. Time
Discharge at 75°F after 7 day stand at 75°F
Note: For clarity, Load 1 surges are shown
at 1 hr. intervals. Actual loading was
a 2-min. load 1 18-min. load 2 cycle.

Specimen No. 11 S/N 78
Date: February 27, 1973



Battery E1 P/N MAP 4435

Discharge Voltage vs. Time

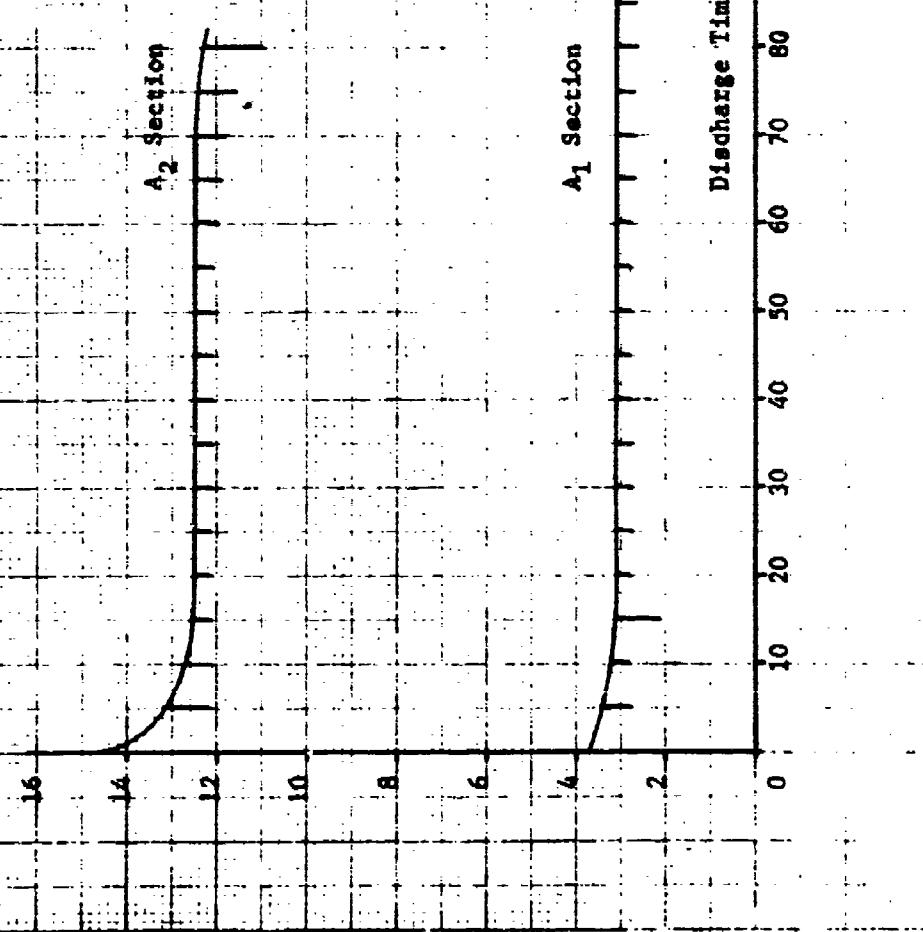
Discharge at 75°F after 7-day stand-at 25°F

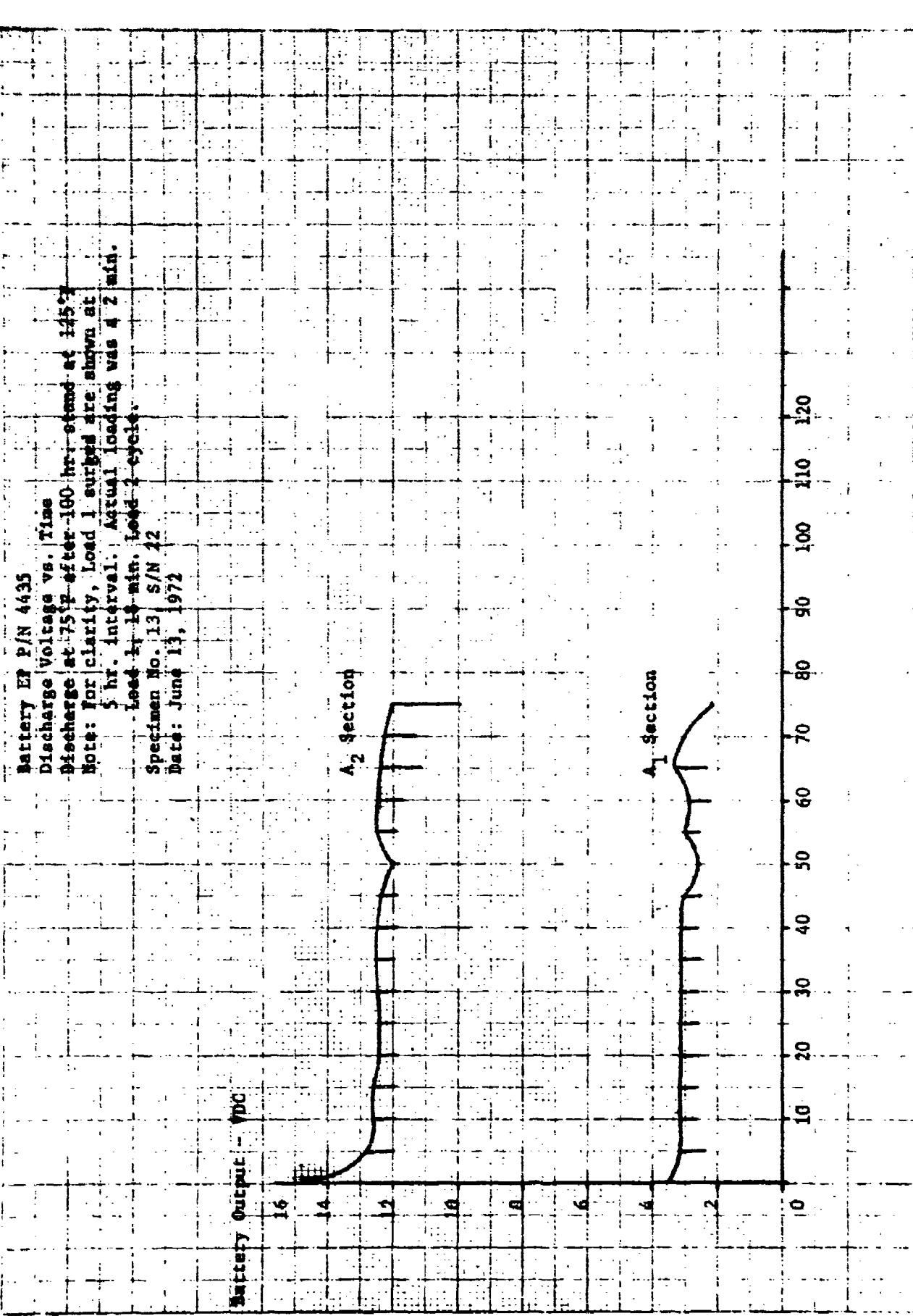
Note: For clarity, Load 1 surges are shown at 5 hr. intervals. Actual load was a 2-min. Load 1, 18-min. Load 2 cycle.

Specimen No. 12, S/N 42

Date: June 13, 1972

Battery Output - VDC





Battery EP P/N MAP 4435

Discharge Voltage vs. Time

Discharge at 75% after 100 hr stand at 100°F

Note: For clarity, Load 1 surges are shown at

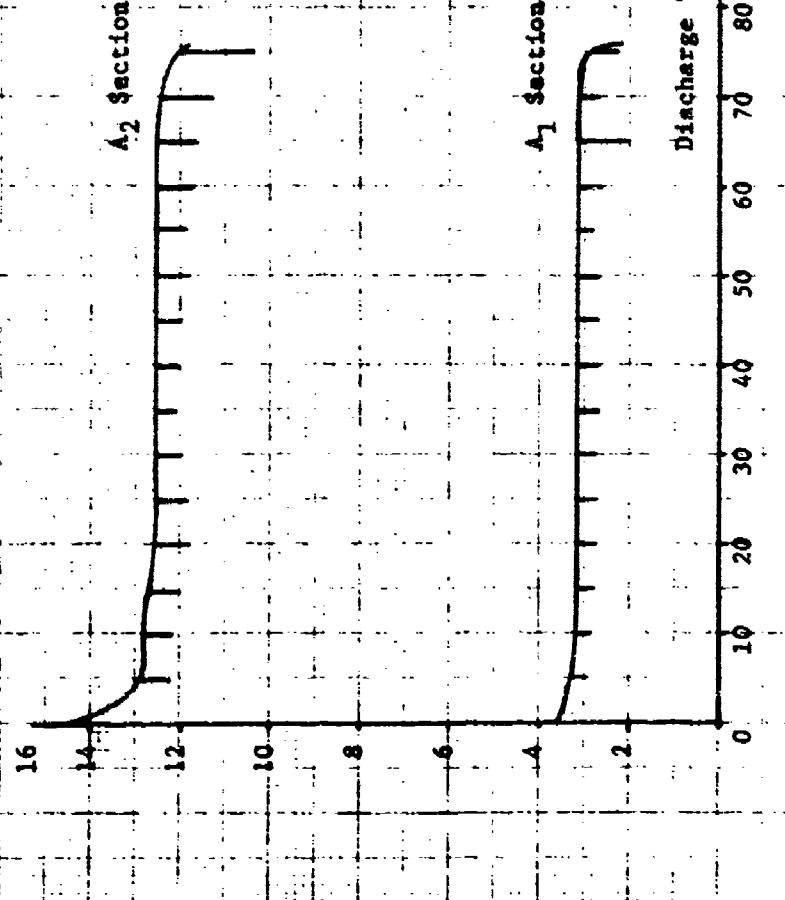
5 hr. intervals. Actual loading was

2 min. Load 1, 18 min Load 2 cycle

Specimen No. 14; D/N 47

Date: October 16, 1972

Battery Output - VDC



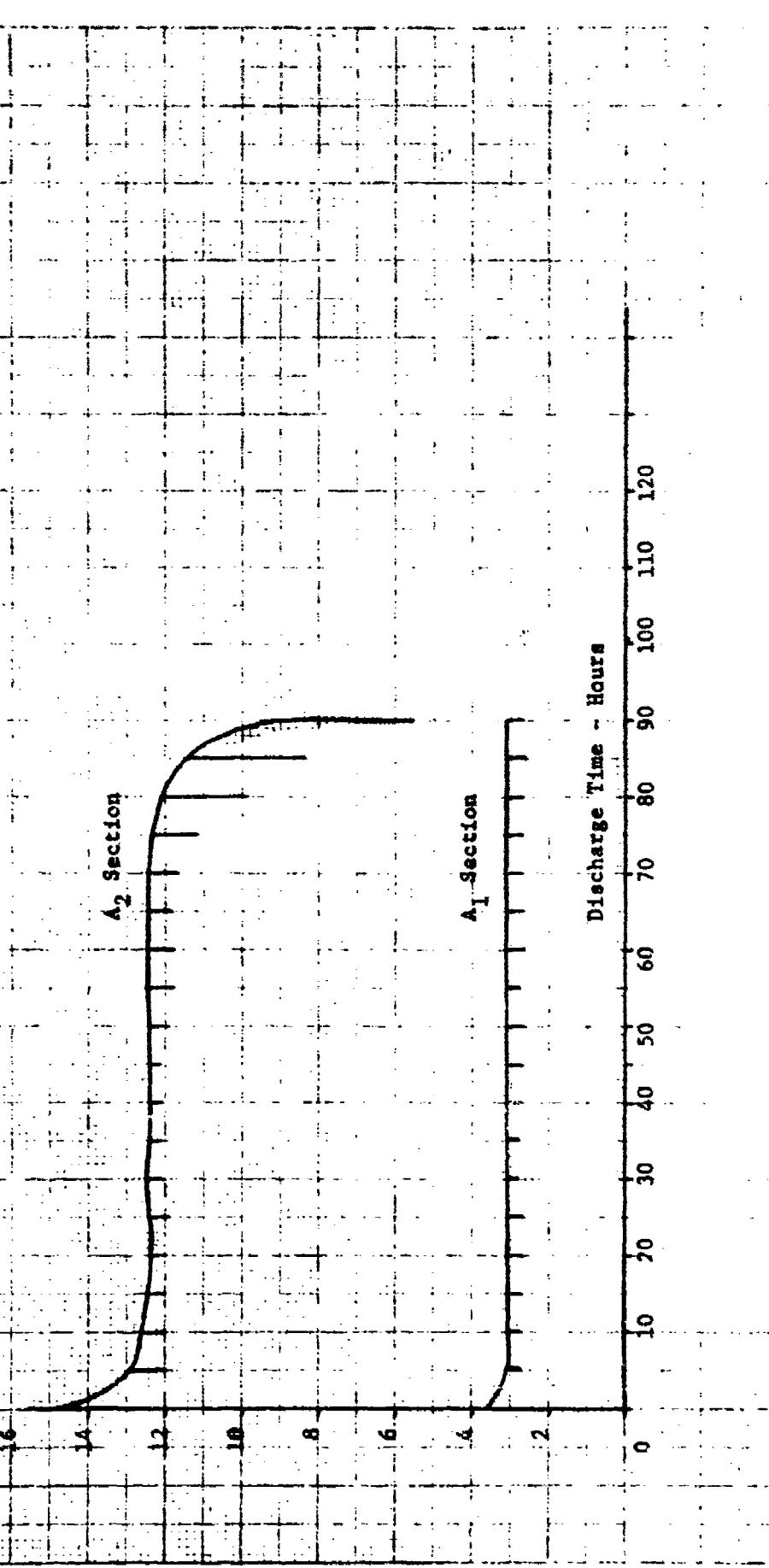
Spec No. 4435 Date 2/26/73

Battery EP P/N MAP 4435
Discharge Voltage vs. Time
Intermediate Discharge at -75° after vibration and shock

Note: For clarity, Load 1 surges are shown at 5 hr.
Intervals: Actual loading was 2.4 min. Load 1
18-min. Load 2.

Specimen No. 15, S/N 74
Date: February 26, 1973

Battery Output - VDC



Battery E P/N MAP 4435

Dielectric Voltage vs. Time

Immediate Discharge at 75°F after Vibration and Shock

Note: For clarity, Load 1 surges are shown at 5 Hz.

Interruption Actual Loading - see [Section A-2](#)

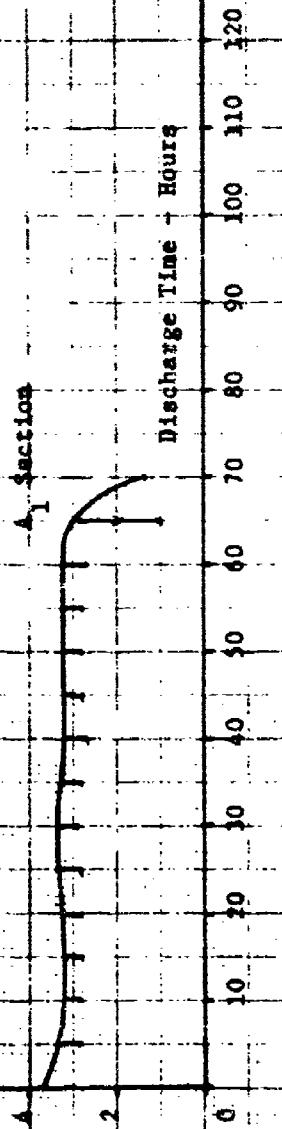
18 min, Load 2 cycle.

Specimen No. 16 S/N 76

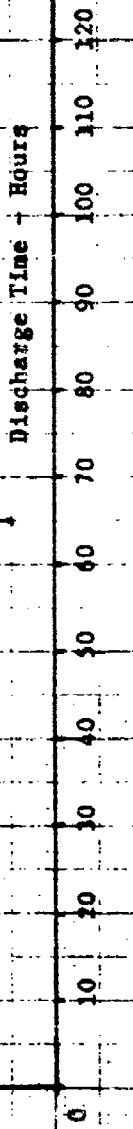
Date: October 17, 1992

BATTERY OUTPUT - VDC

A₂ Section



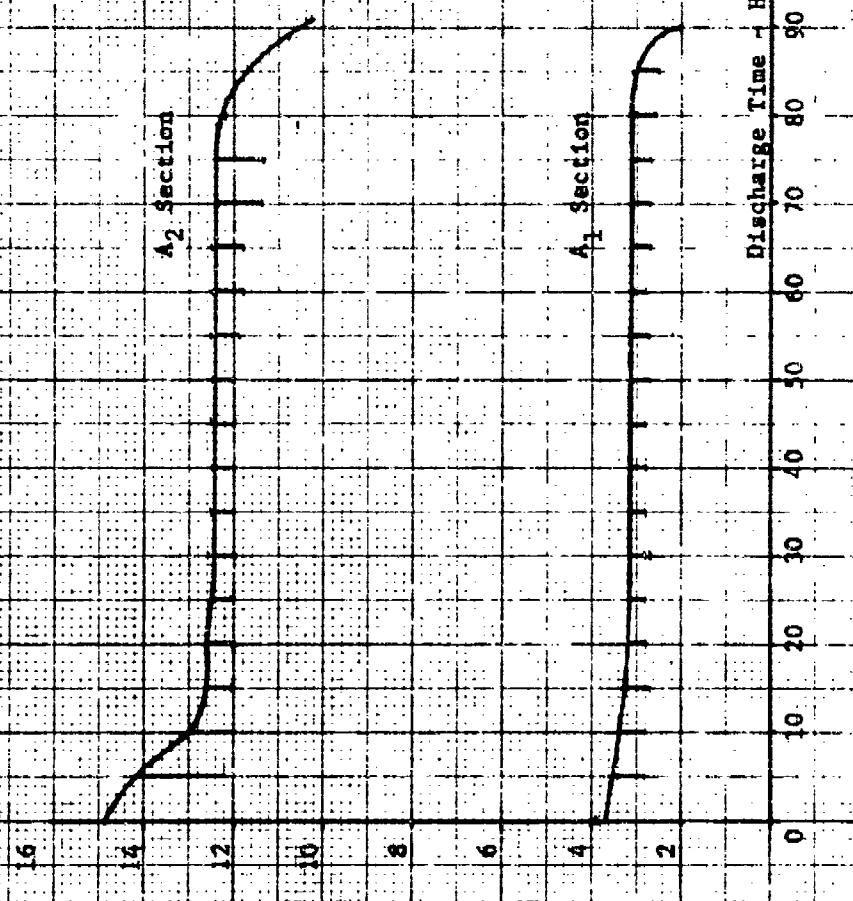
A₁ Section



H-E INSTRUMENTS INC.
KINETIC TEST EQUIPMENT

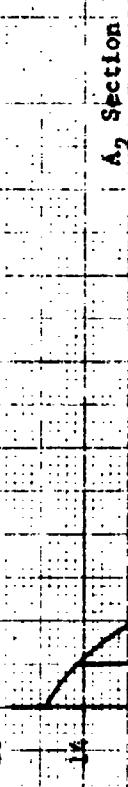
Battery EP P/N NAP 4435
Discharge Voltage vs. Time
Immediate Discharge during Mechanical Shock
Note: For clarity, Load 2 curves are shown at
5 hr. Intervals. Actual loading was a
2 min. Load 1, 18 min. Load 2 cycle
Specimen No. 17 S/N 3
Date: June 19, 1972

DISCHARGE TIME - HRS.

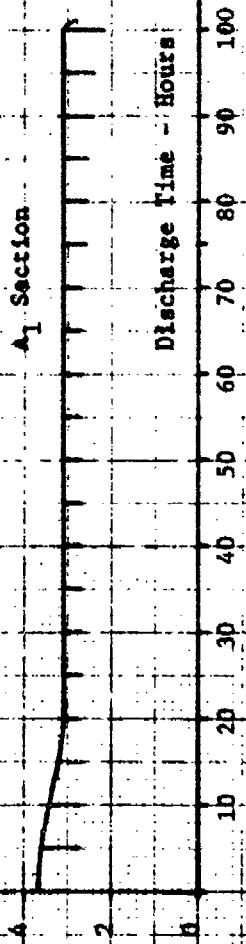


Battery EP P/N MAP 4435
Discharge Voltage vs. Time
Immediate Discharge during Mechanical Shock
Note: For clarity, Load 1 surges are shown at
5 hr intervals. Actual loading was
2 min. Load 1, 10 min. Load 2 cycle.
Specimen No. 18, S/N 7
Date: June 19, 1972

Battery Output = VDC

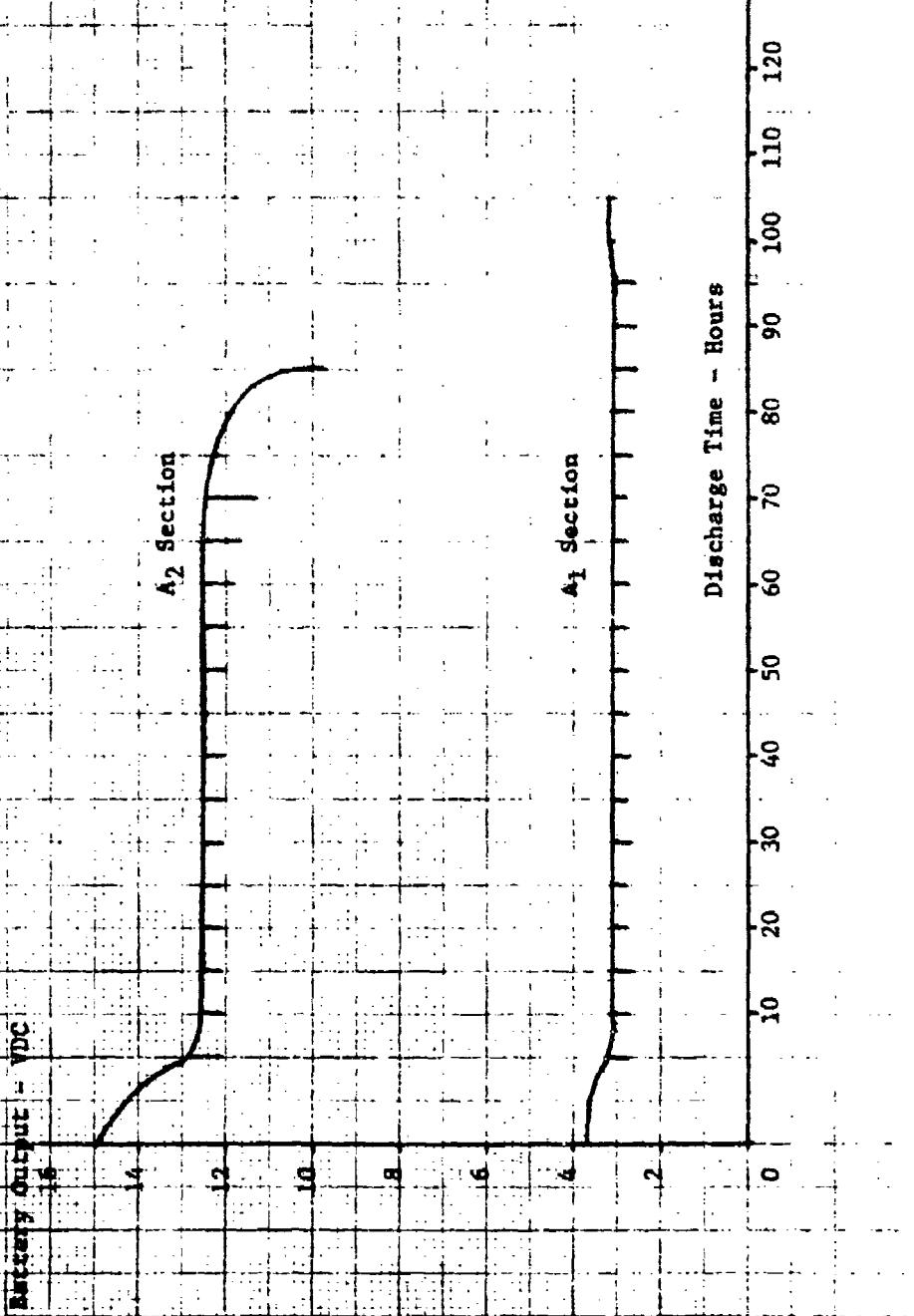


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Specimen No. 19, S/N 8
Date: June 19, 1972

Battery EB P/N MAP 4435
Discharge Voltage vs. Time
Immediate Discharge during Vibration
Note: For clarity, Load 1 surges are shown at
5 hr. intervals. Actual loading was a
2-min. Load-1, 18-min. Load-2 cycle.
Specimen No. 19, S/N 8
Date: June 19, 1972



Battery EP P/N MAP 4435

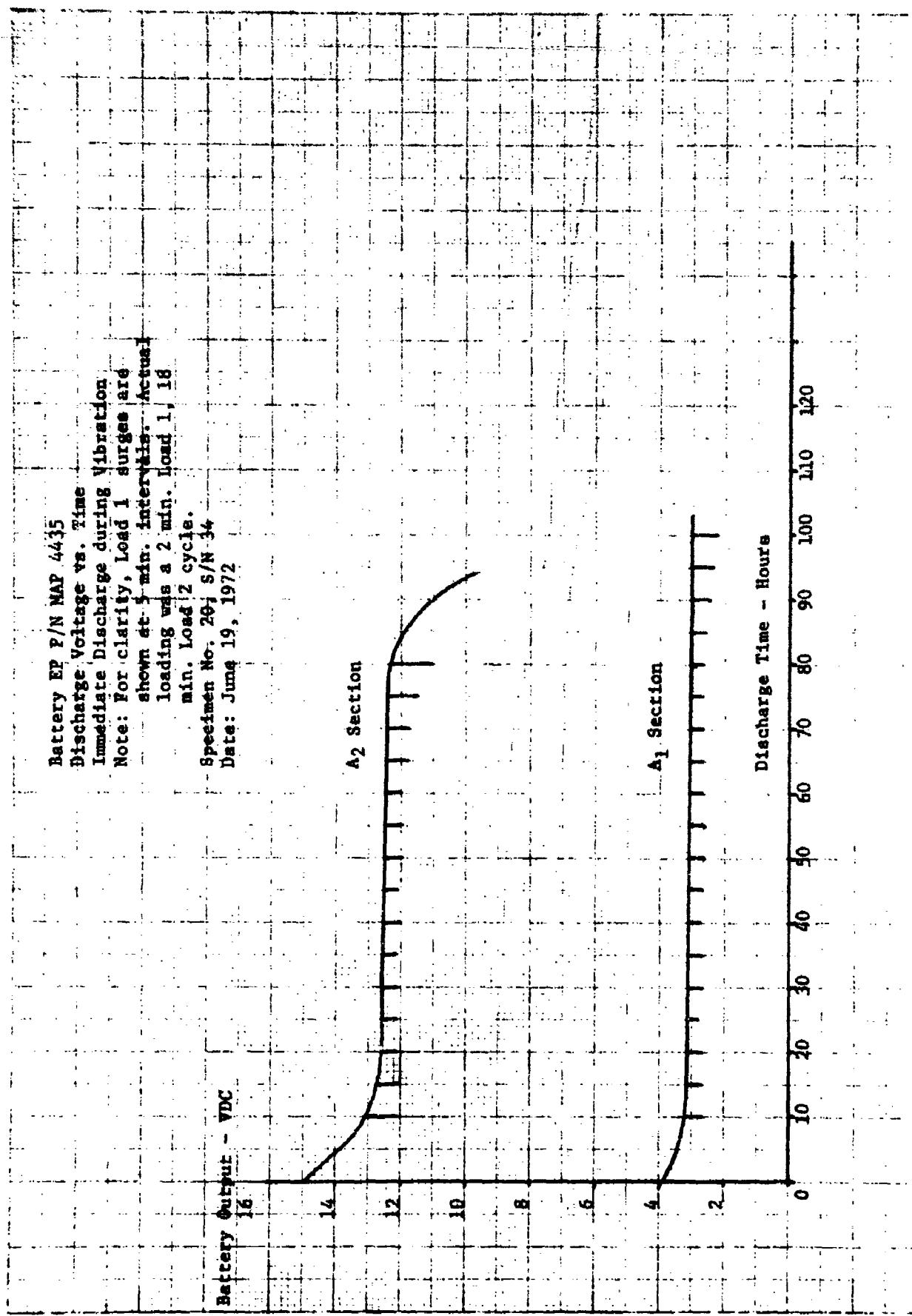
Discharge Voltage vs. Time

Immediate Discharge during Vibration

Note: For clarity, Load 1 surges are shown at 5 min. intervals. Actual loading was a 2 min. load 1 18 min. load 2 cycle.

Specimen No. 20; S/N 34

Date: June 19, 1972

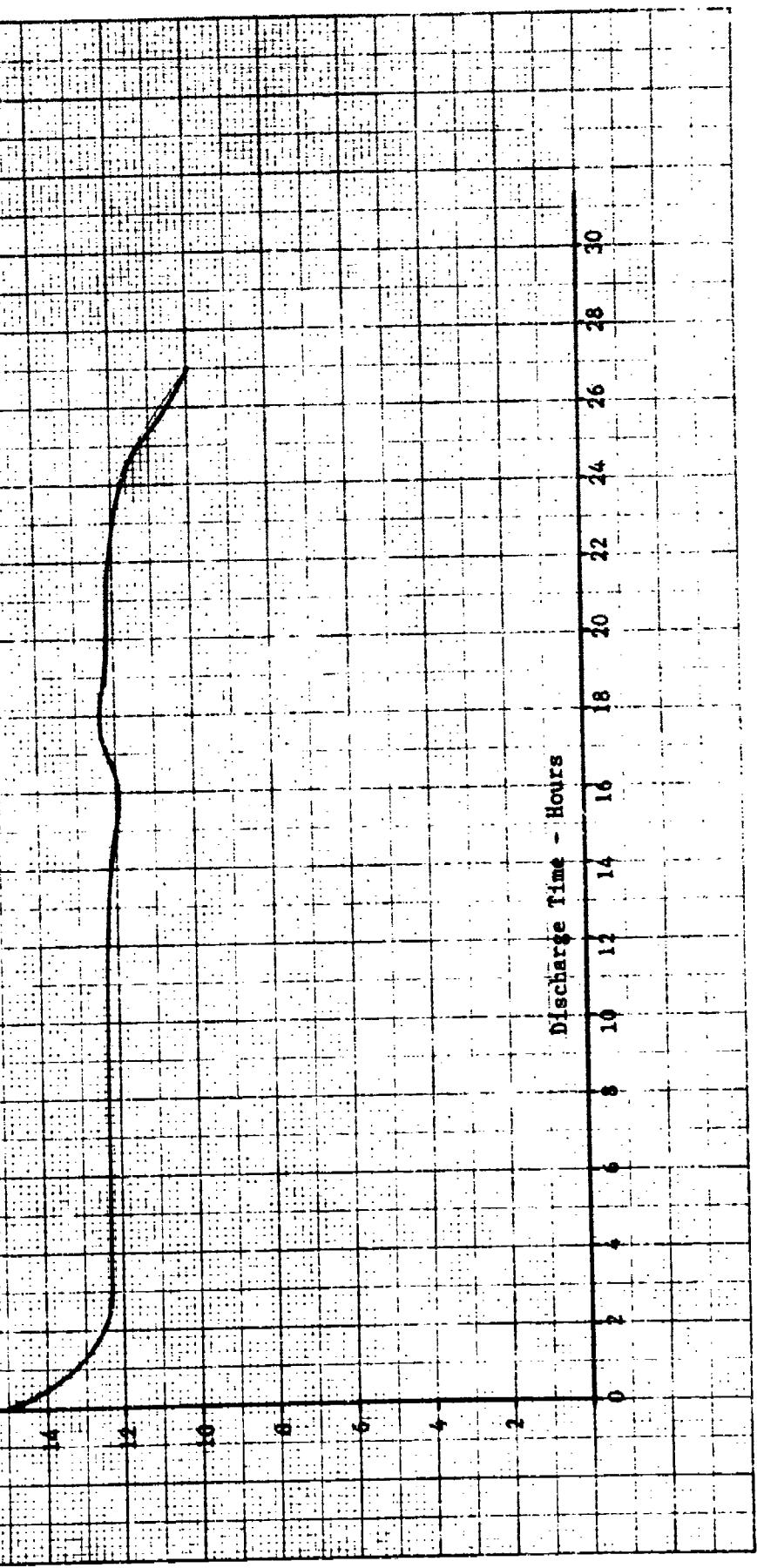


KEE
KELLEER ELECTRIC COMPANY
P.O. BOX 1323

Battery P/N MAP 51474
Discharge Voltage vs. Time
Immediate Discharge at 75°F
Specimen No. 21, S/N 9
Date: June 5, 1972

Time

Battery voltage - mV



Battery BP P/N MAP 4435

Discharge Voltage vs. Time

Immediate Discharge at 75°F

Specimen No. 22, S/N 18

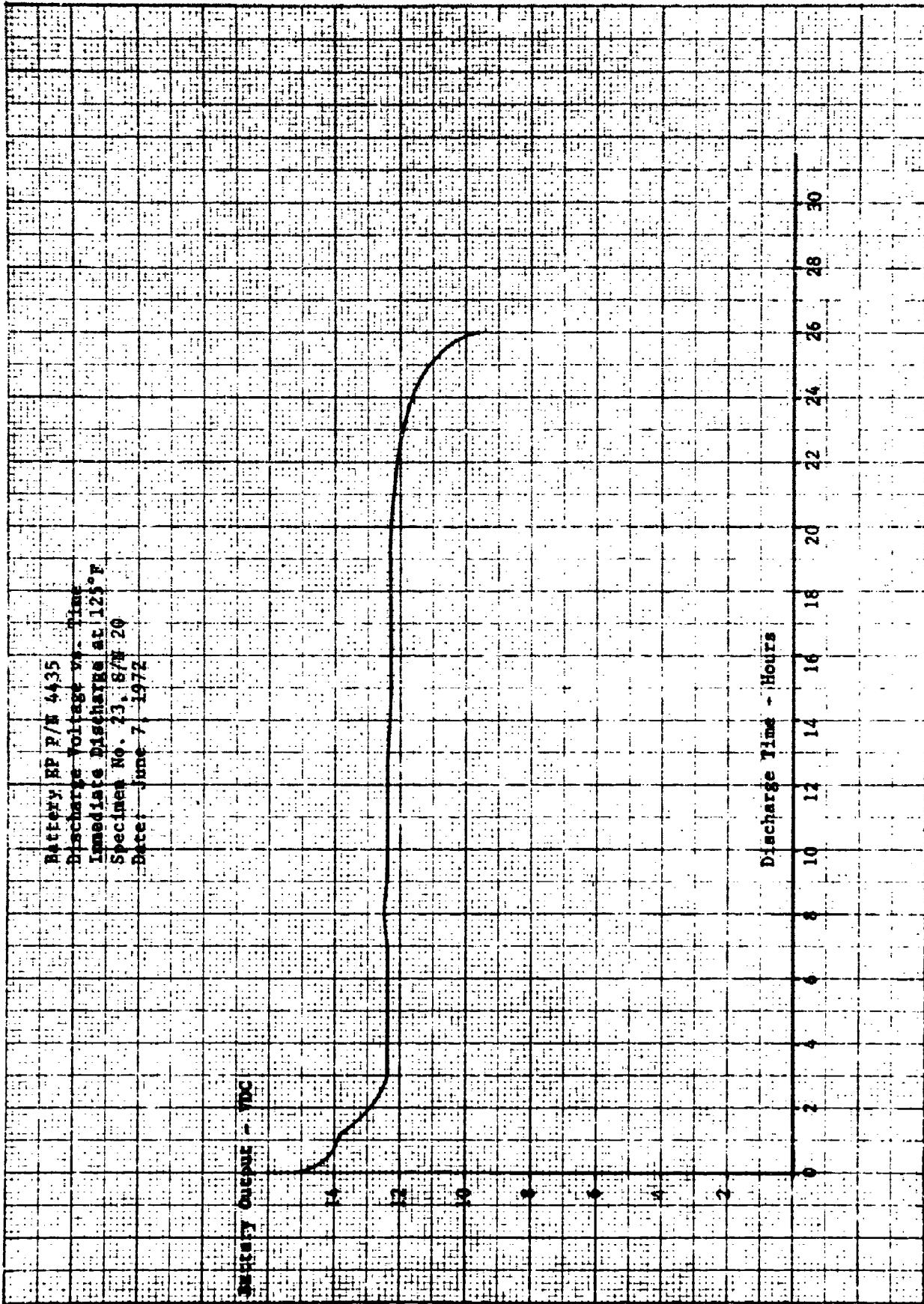
Date: June 5, 1972

Voltage Output - VDC

Discharge Time - Hours

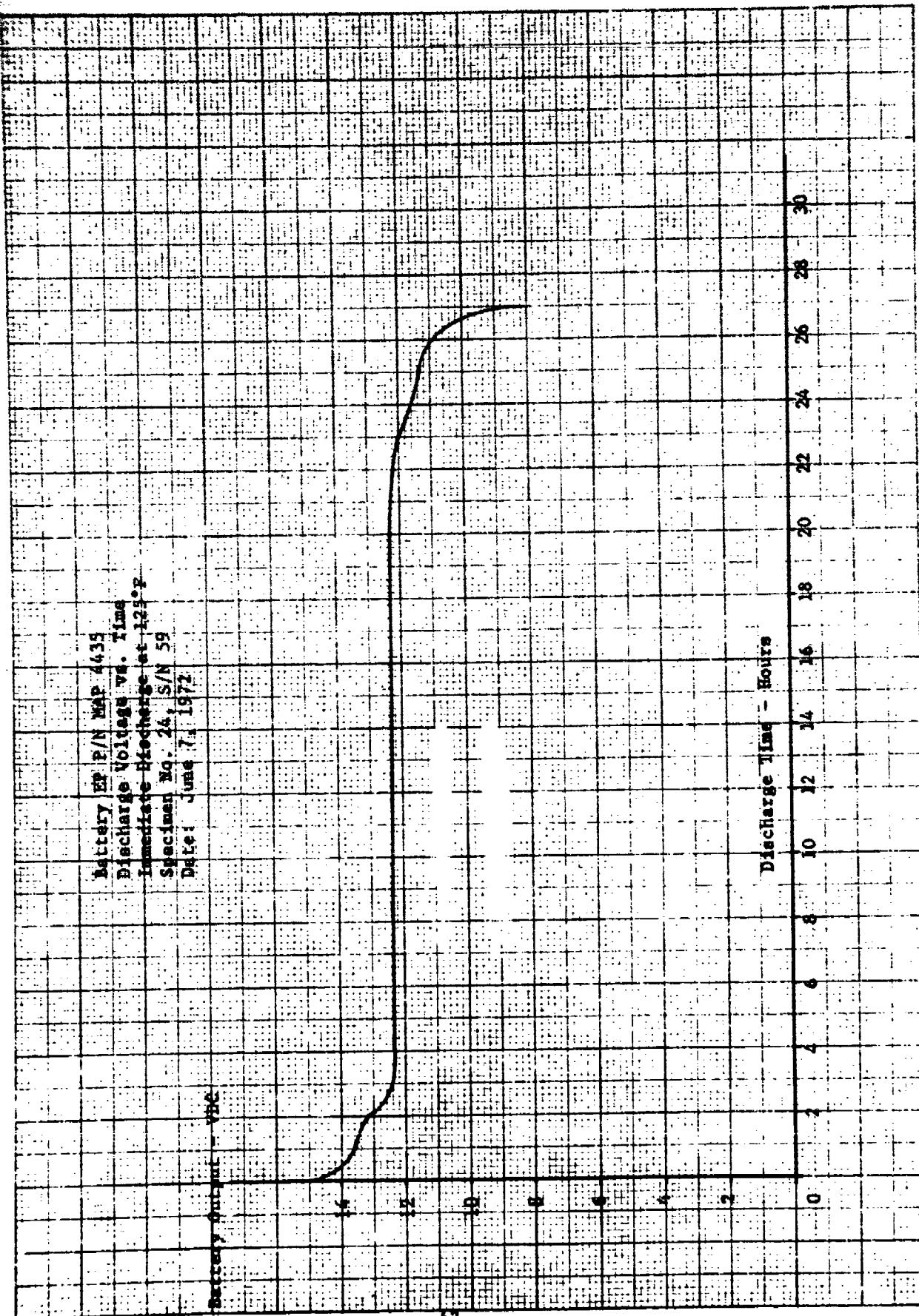
0	2	4	6	8	10	12	14	16	18	20	22	24	26	28	30
---	---	---	---	---	----	----	----	----	----	----	----	----	----	----	----

K-E
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SERIAL • 81553



Battery E2 P/N MA2 4439
Discharge Voltage vs. Time
Instrument Model - 1230-2
Specimen No. 24 S/N 59
Date: June 7, 1972

Discharge Time - Hours
20 22 24 26 28 30
18 16 14 12 10 8
16 14 12 10 8 6
14 12 10 8 6 4
12 10 8 6 4 2
10 8 6 4 2 0



H.E. OXIDE INC. 48123
KODAK SAFETY FILM
KODAK SAFETY FILM

Battery Output - VDC

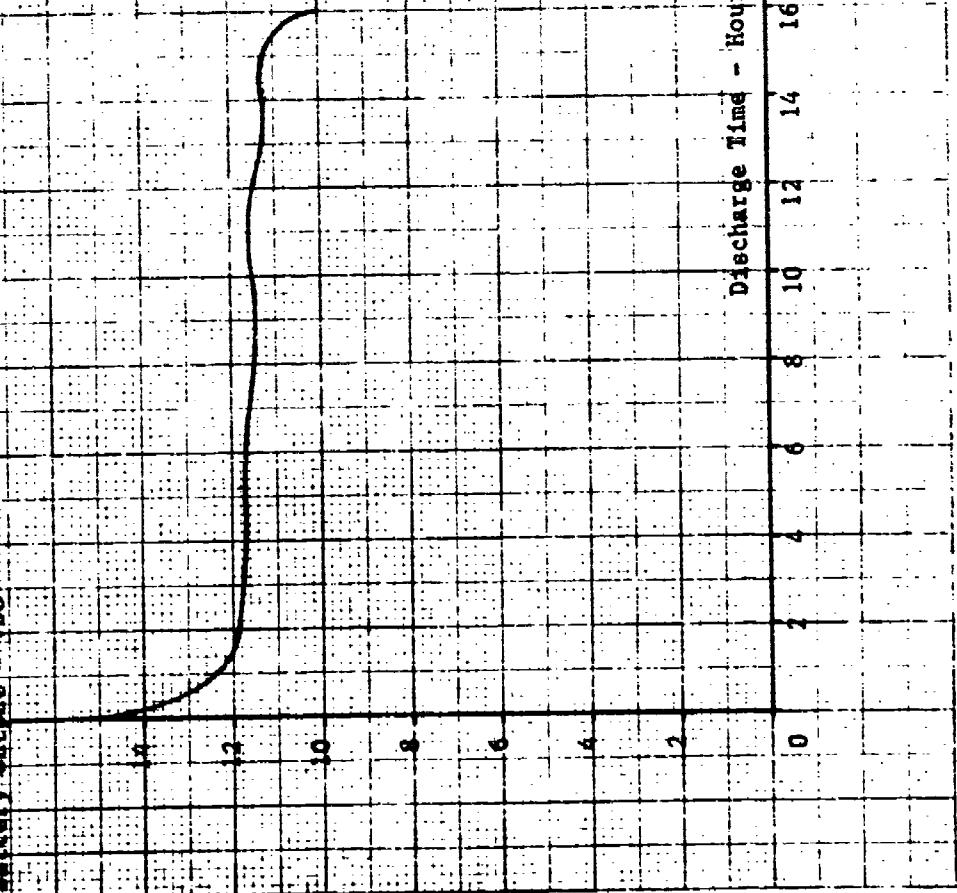
Discharge Voltage vs. Time

Immediate Discharge at 0°

Specimen No. 25-37A-11

Date: March 8, 1973

Battery Output - VDC



Battery EP P/N MAP 4435
Discharge Voltage vs. Time
Instantaneous Discharge rate 0°F
Specimen No. 26, S/N 31
Date: June 14, 1972

Battery Model 4435

Discharge Time - Hours
0 1 2 3 4 6 8 10 12 14 16 18 20 22 24 26 28 30



28

Discharge - Cubic Feet Per Second

Discharge Time - Hours

2

4

6

8

10

12

14

16

18

20

22

24

26

28

30

32

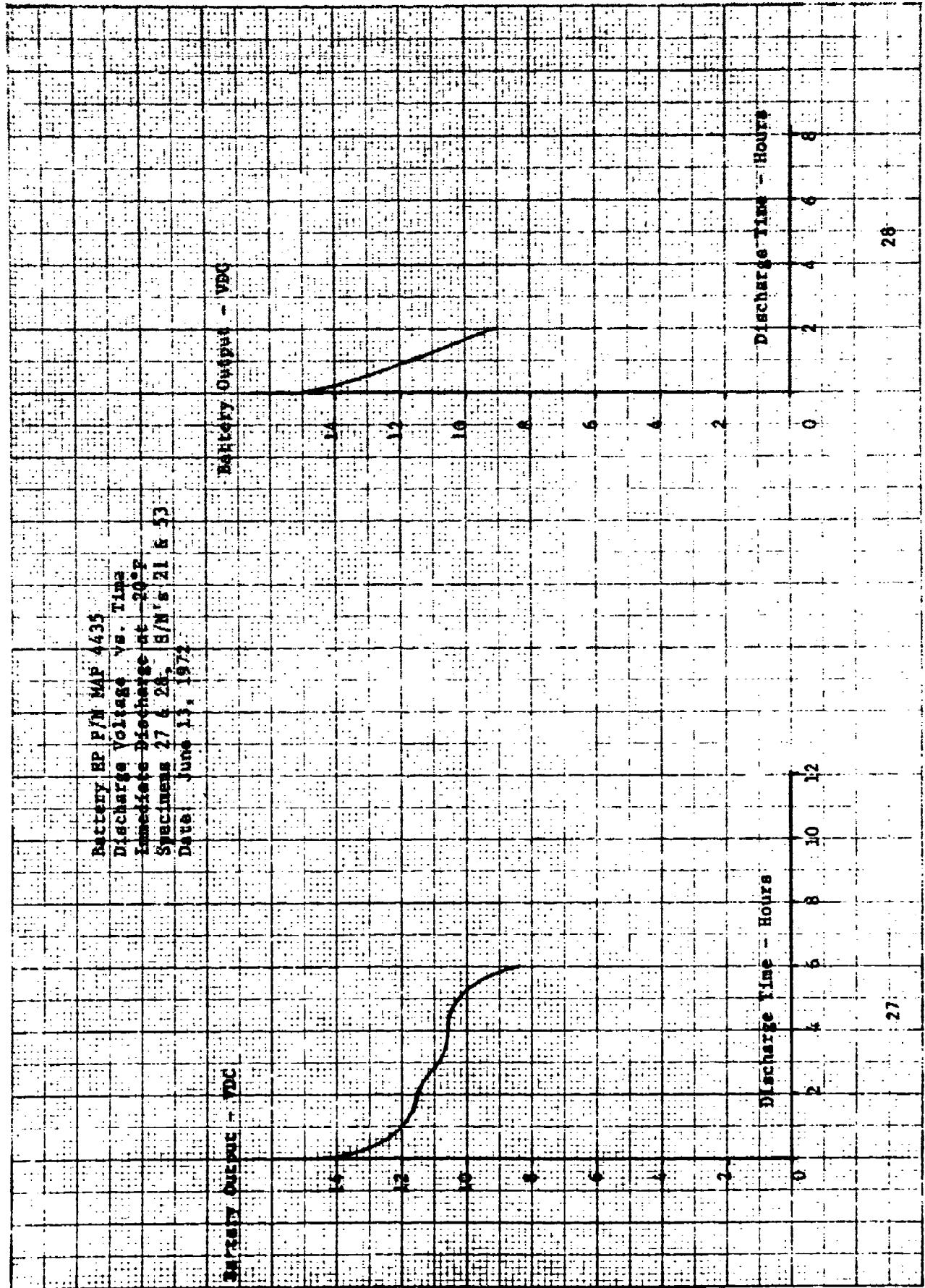
34

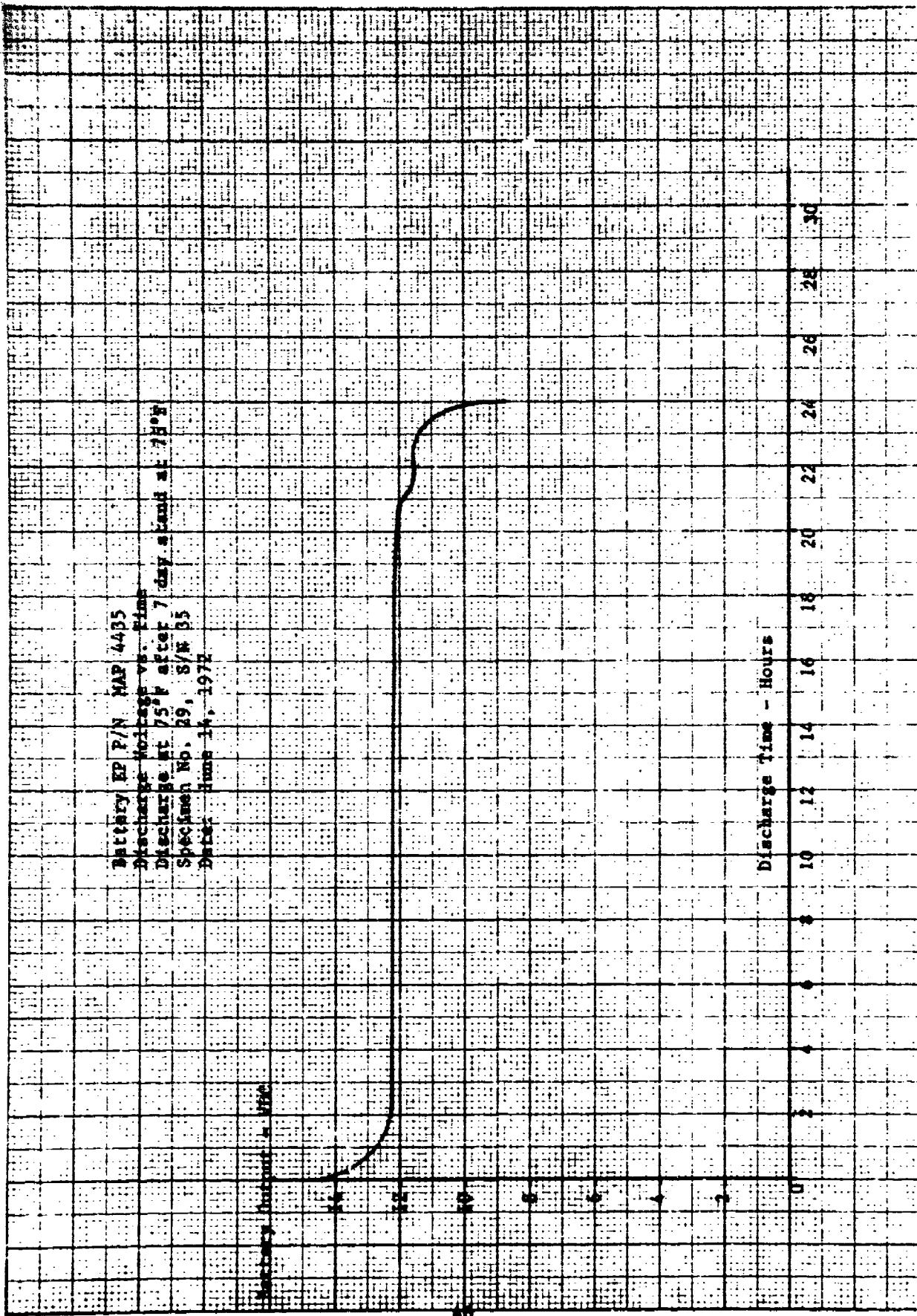
27

Data - Hydrograph

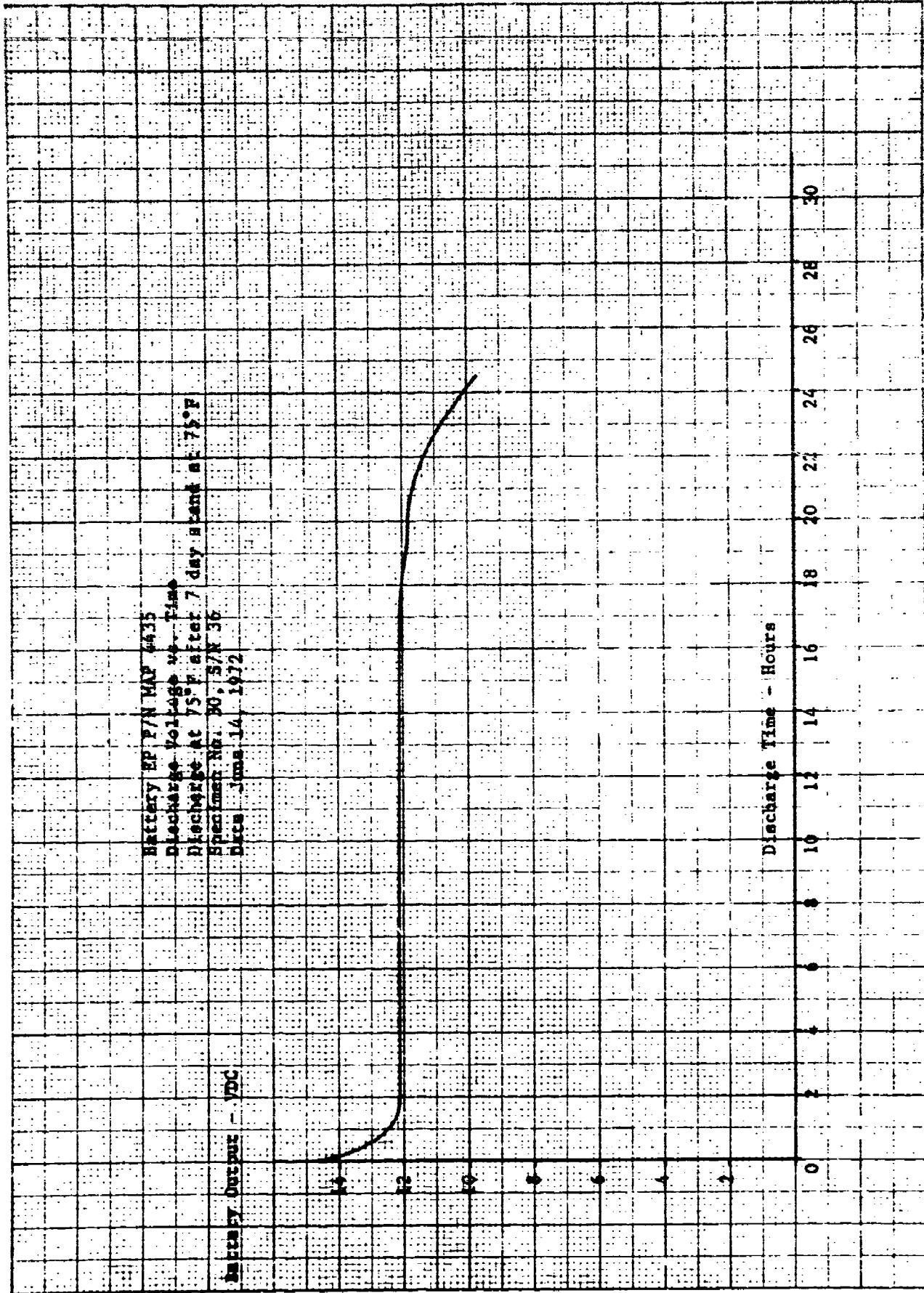
Data - Dose

Date: June 13, 1972
 Discharge: 27 CFS
 Discharge Duration: 4 hours
 Velocity: 0.7 ft/sec





H-E
KODAK SAFETY FILM
EXPIRED OCTOBER 1972



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13. ABSTRACT This report describes the design, development, manufacture and evaluation testing of a Zinc-Silver Oxide reserve battery in accordance with "Technical Guidelines for Water Activated Zinc-Silver Oxide Battery". This includes a description of the design effort, the design, the test program, the test equipment and the test results. The evaluation testing showed compliance with the requirements of the technical guidelines.		

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